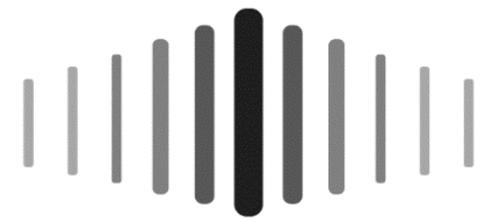


Resilient and Robust PNT

Todd Humphreys

With input from Peter Iannucci, Matthew Murrian, and Lakshay Narula
The University of Texas at Austin Radionavigation Lab



THE UNIVERSITY OF TEXAS AT AUSTIN
RADIONAVIGATION LABORATORY

All material in this presentation is drawn from the open literature. References are provided within and at the end of the presentation.



Fortunately

by REMY CHARLIP



50¢
T3-817



unfortunately



4 billion GNSS devices in use globally

GSA 2015 market report

Core global revenue due to GNSS: \$76B

GSA 2015 market report

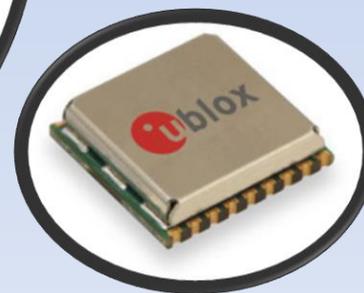
Enabled global revenue due to GNSS: \$278B

GSA 2015 market report

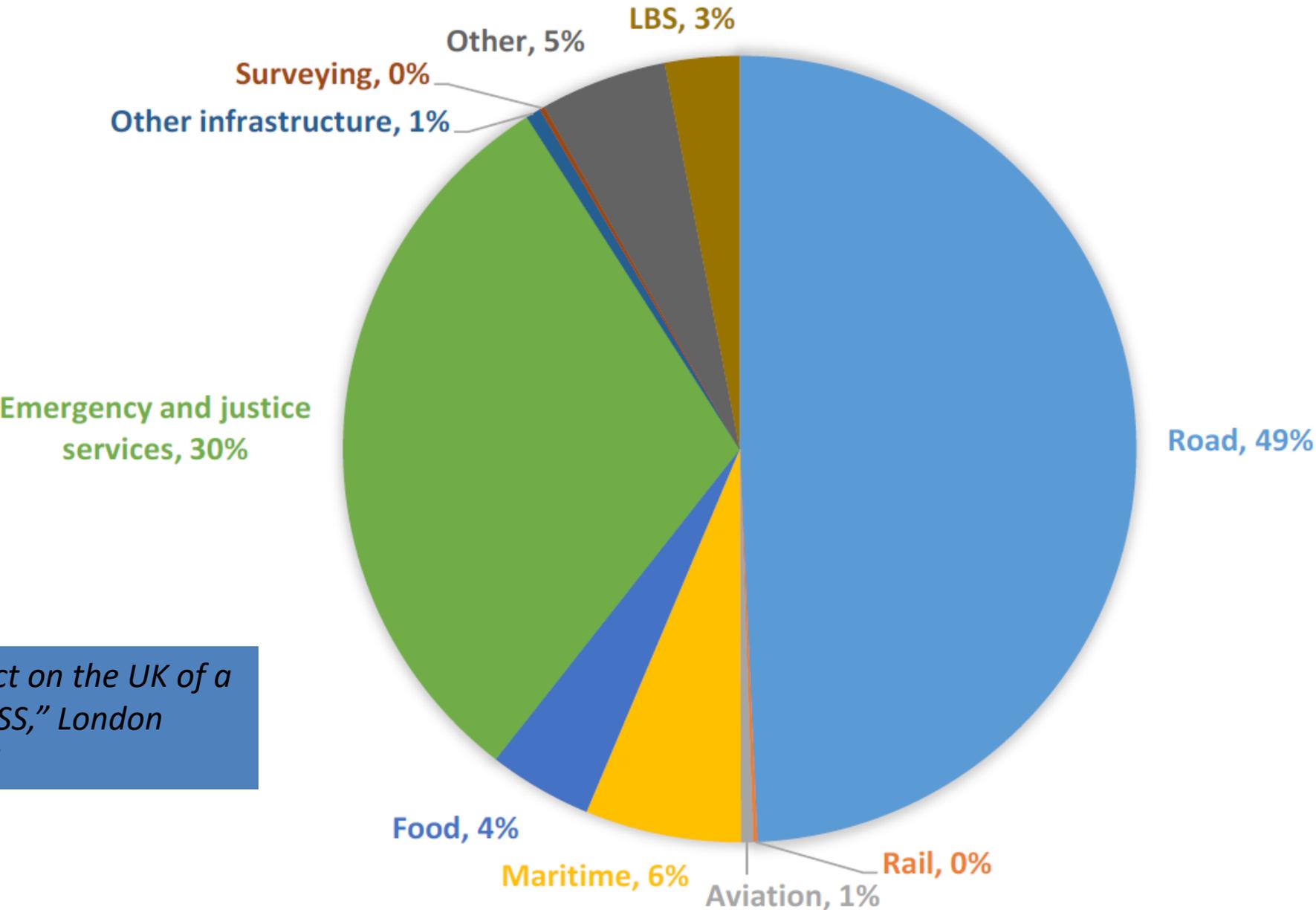
Economic cost to UK of 5-day GNSS outage: \$7.2B

"Economic Impact on the UK of a disruption to GNSS," London Economics, 2017





GNSS BENEFITS



“Economic Impact on the UK of a disruption to GNSS,” London Economics, 2017

Q: Will GNSS remain the pre-eminent worldwide source for positioning, navigation, and timing (PNT)?

A: Unfortunately, serious GNSS vulnerabilities need addressing; these may be unfixable.

Two schools of thought:

(1) Fix GNSS

**(2) Seek stand-alone
alternative sources of PNT**

PTA

**Protect
Toughen
Augment**

APNT

**Alternative
Positioning
Navigation
Timing**



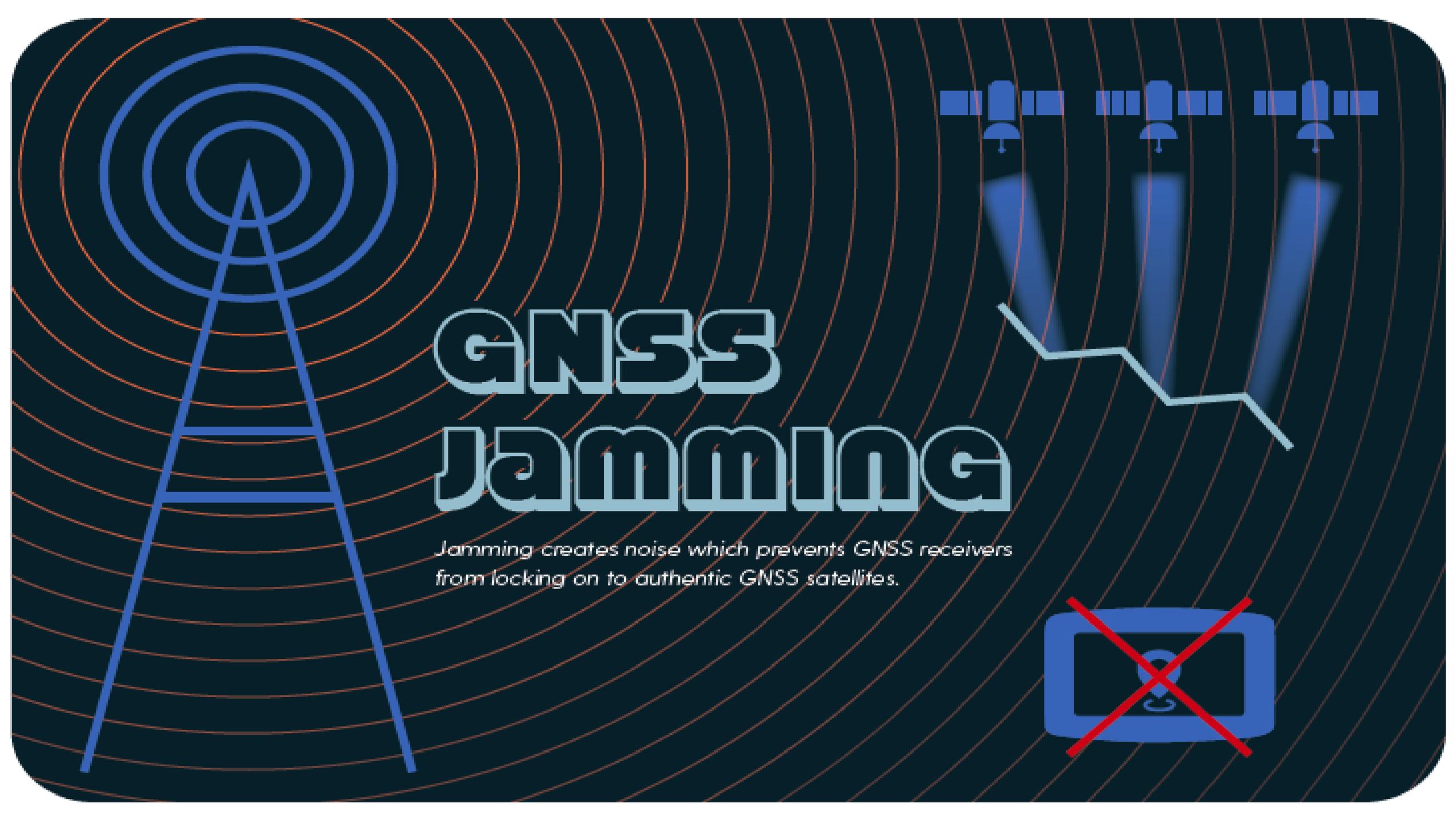
“Needed: About 35 dB of additional receiver interference resistance.”

Bradford Parkinson, Architect of GPS, “Nibbles,” 2012



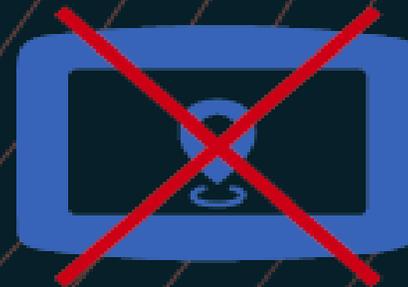
“... we’re looking beyond GPS ... we need to find alternatives for military use that are more resilient and less vulnerable.”

Former Sec. Defense Ash Carter giving Drell Lecture at Stanford in 2015



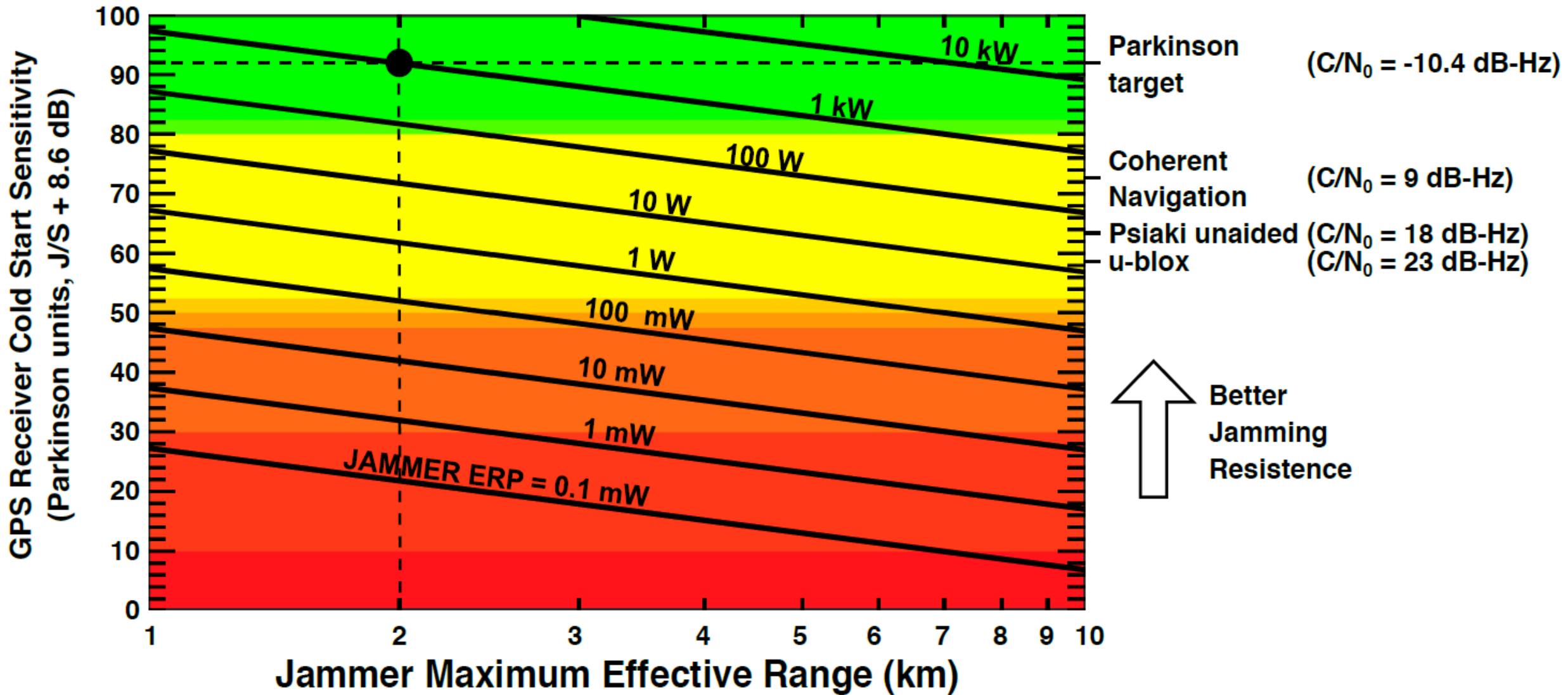
GNSS JAMMING

Jamming creates noise which prevents GNSS receivers from locking on to authentic GNSS satellites.



1 kW wideband jammer can deny service to the best COTS GNSS receivers over a ~200 km (line-of-sight) effective range





PTA: By (1) deep coupling with inertial sensors, and (2) multi-element antennas we can toughen GNSS receivers enough to withstand 1 kW wideband Gaussian jammer at a distance of 2 km.

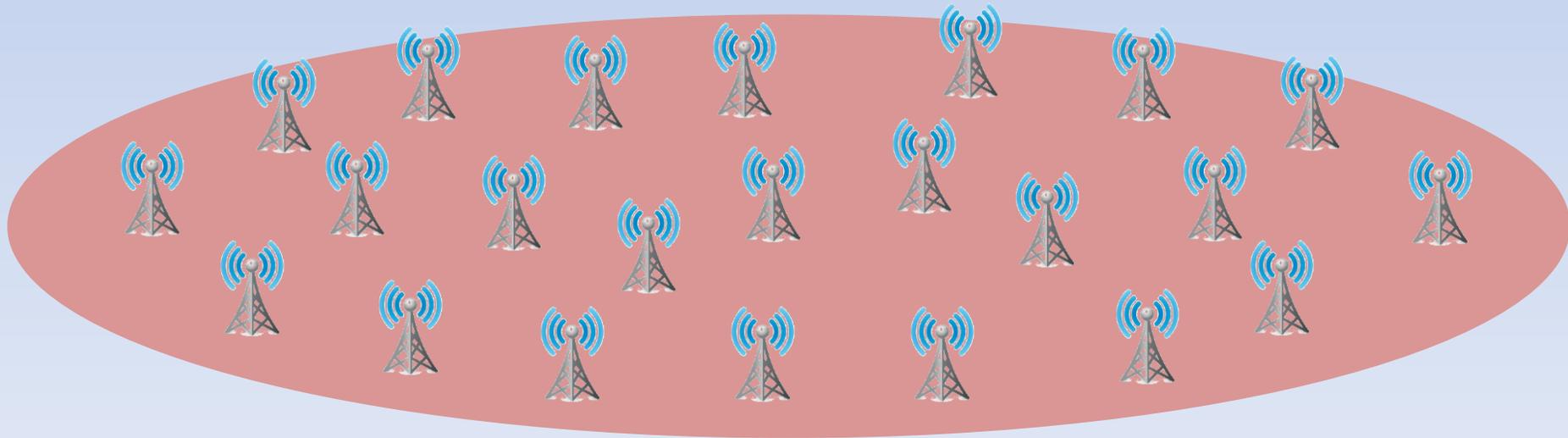
Deploying full combination of best current technology
could shrink effective range to 2 km.
Moreover, the jammer itself becomes a counterstrike target.



But cost asymmetry favors the jammer:

1 kW jammer cost: ~\$200

Cost for enough jammers to deny service in 200-km-radius zone: ~\$2 M

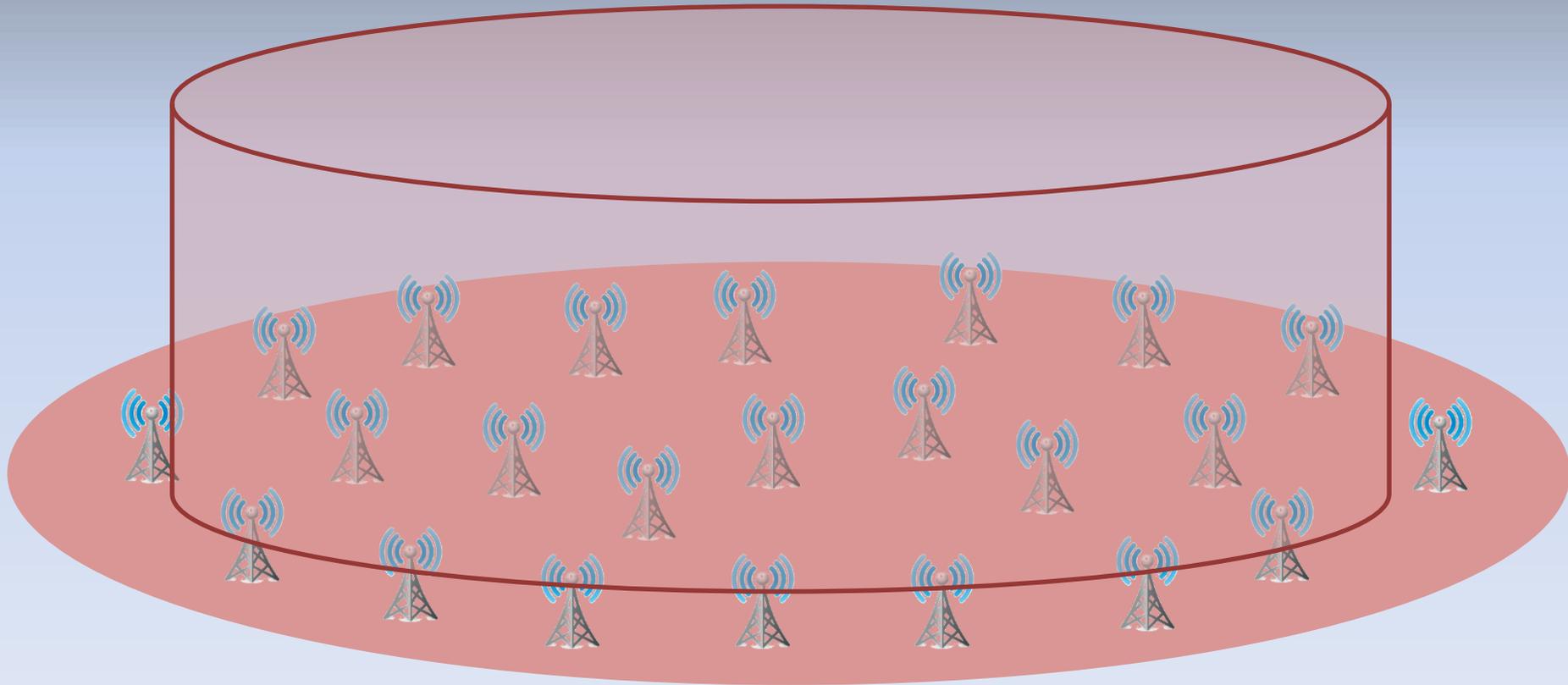


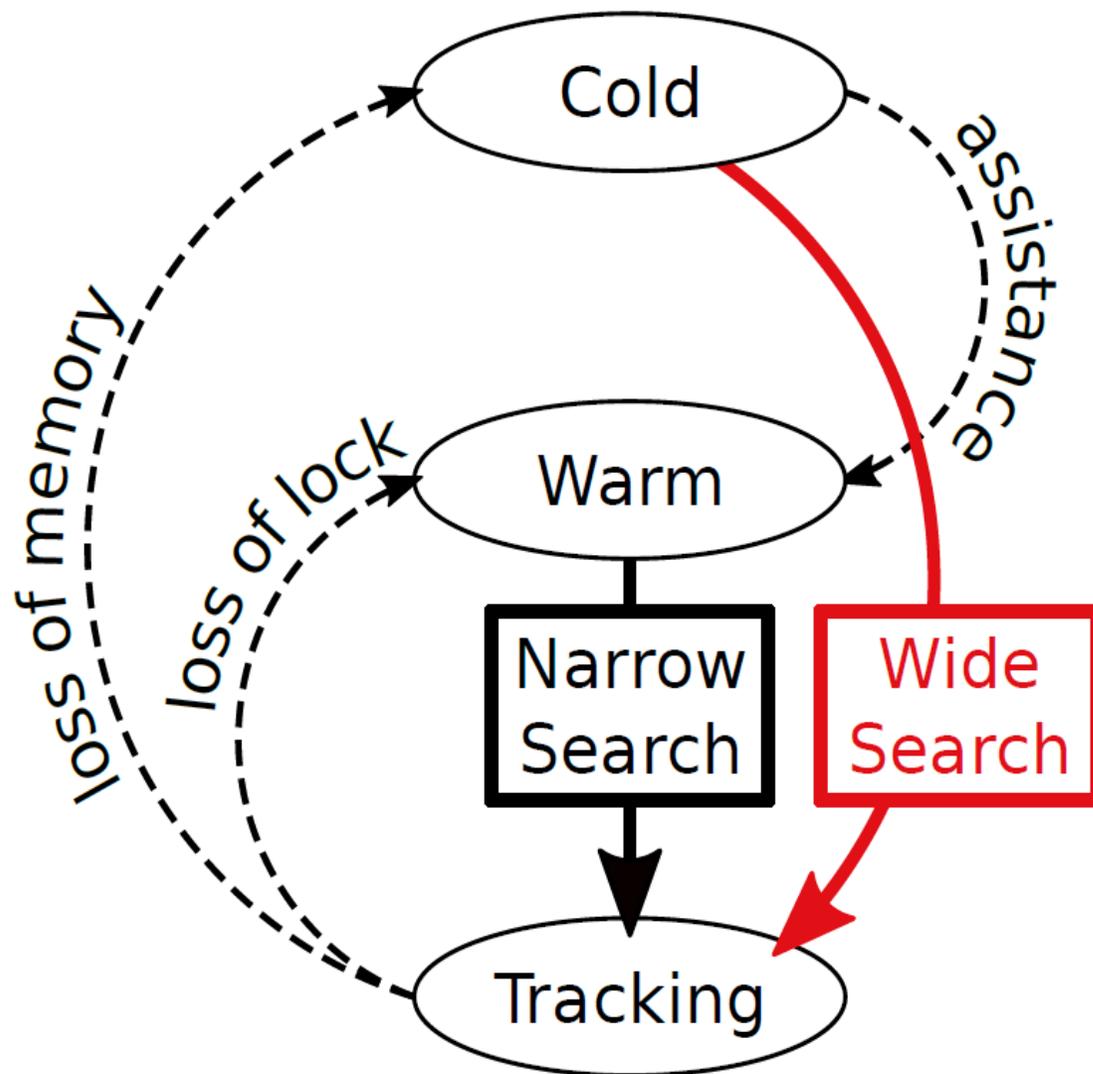
But cost asymmetry favors the jammer:

1 kW jammer cost: ~\$200

Cost for enough jammers to deny service in 200-km-radius zone: ~\$2 M

Jamming power now remains constant with altitude





What is more, immunity to J/S = 84 dB jamming environment almost certainly requires warm start for encrypted (non-repeating) wideband codes such as M-code: side channel must provide approximate time and location.

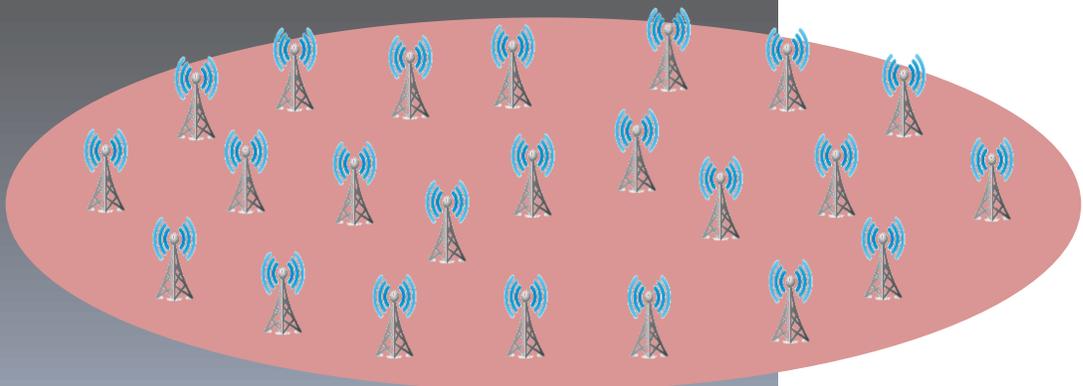
GPS L1 CA PRIMARY

1	19u	-29228.2	-0.0	0.0	39.3	359.4	-75.1	5*
2	5u	-29228.2	-0.0	0.0	40.2	54.9	-38.4	5*
3	12u	-29228.7	-0.0	0.0	41.3	107.6	-47.8	5*
4	17u	-29226.3	-0.0	0.0	42.9	341.0	-59.1	5*
5	2u	-29227.7	-0.0	0.0	42.5	112.4	-58.6	5*
6	1u	-29226.9	-0.0	0.0	40.2	281.5	-17.5	5*
7	4	-31420.0	2097925.9	23905339.5	42.1	196.6	-4.0	6
8	16	-40379.6	2650169.5	21204591.2	40.5	220.0	10.2	6
9	18	-25577.3	1688476.6	21204591.2	40.5	220.0	10.2	6
10	22	-34506.5	2316331.2	21204591.2	40.5	220.0	10.2	6
11	7	-16254.9	811922.4	24880641.3	27.3	313.7	-15.2	6-
12	8	-10484.9	76068.5	20159639.2	32.0	311.3	29.4	6
13	10	-7468.0	328301.5	17415104.7	38.9	227.7	79.1	6

“Coded” jammer uses authentic spreading codes

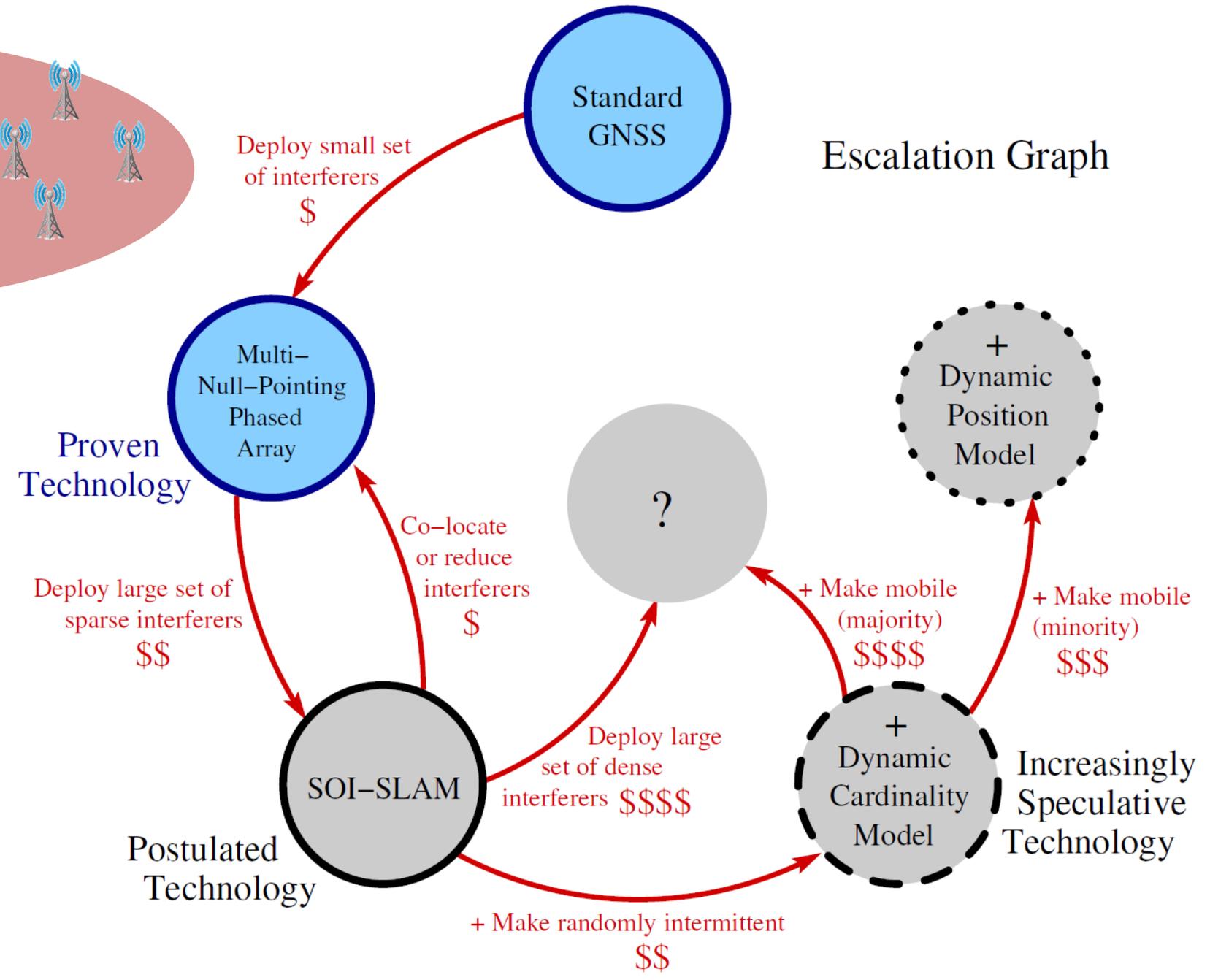
A coded jammer (or meacon) is more potent than uncorrelated wideband jammer: Each coded signal produces a correlation peak competitor that must be distinguished from authentic peak.

Upshot: even 35 dB of additional interference resistance (expensive!) would not prevent a determined adversary from cost-effectively denying GNSS over an area the size of Colorado.



The “fortunately, unfortunately” game can be played with distributed jamming technology: the defender can use the jamming sources as beacons in a “Signal of Opportunity from Interference (SOI) Simultaneous Localization and Mapping (SLAM)” framework.

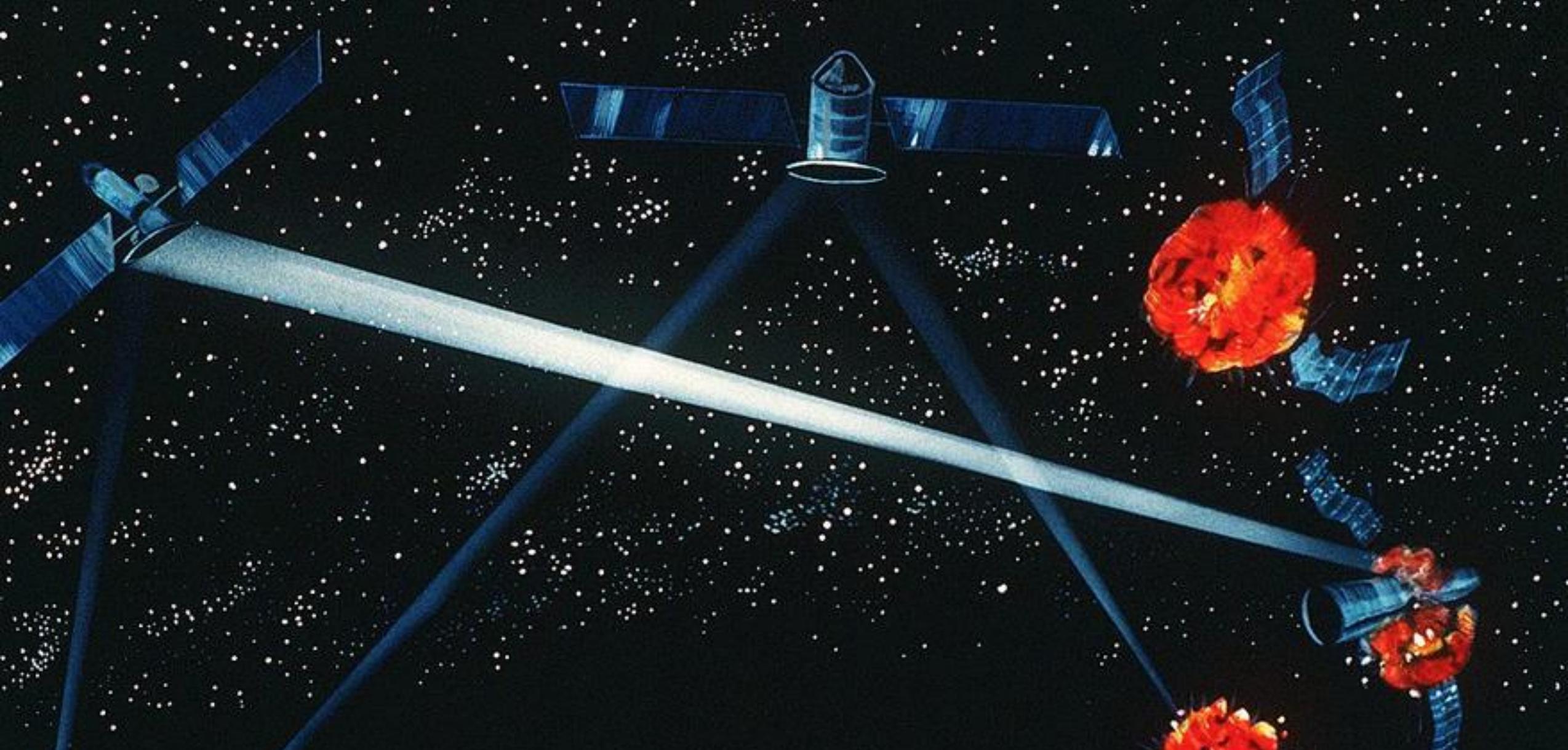
Escalation Graph



**Q: Could directed energy weapons damage
GNSS satellites?**



Directed energy: current technology could jam but not damage: Recently-completed Chinese FAST radio telescope is largest in world: 300-meter diameter steerable aperture. If used to focus energy of a massive 466 MW magnetron, power flux at MEO would be only 20 Watts per square meter, less than 1/50 of solar irradiance.



Directed energy: future technology (e.g., space lasers)
could damage GNSS satellites



“[An influential view within China] is that this next phase [of warfare] will be characterized by combining manipulations of “Big Data” and increasing autonomy/artificial intelligence, with directed energy weapons at the core.”

**Q: Could direct-ascent kinetic ASAT
weapons destroy GNSS satellites?**

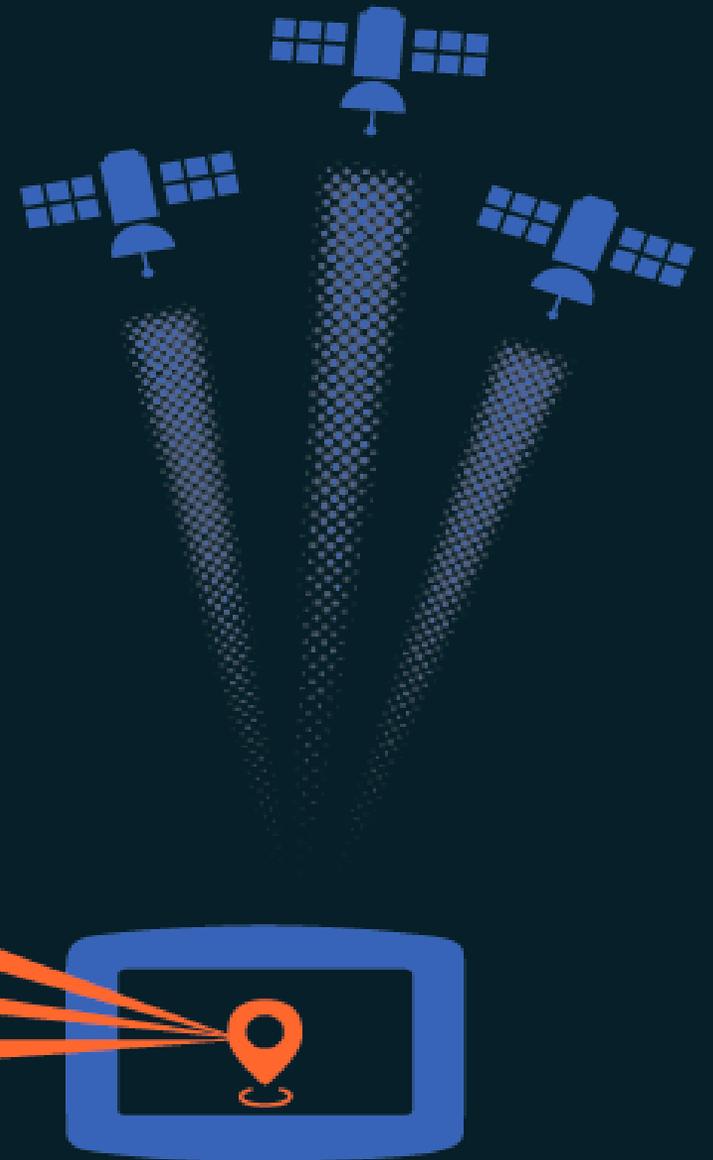
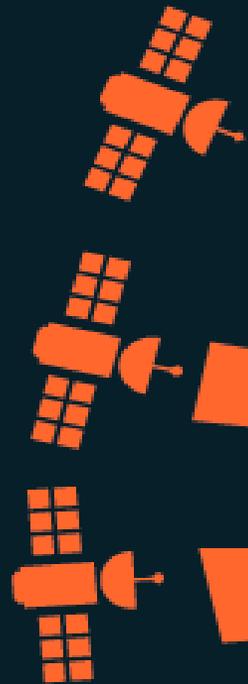
May 2013: Chinese launched experimental direct-ascent ASAT weapon that reached beyond GPS orbit.



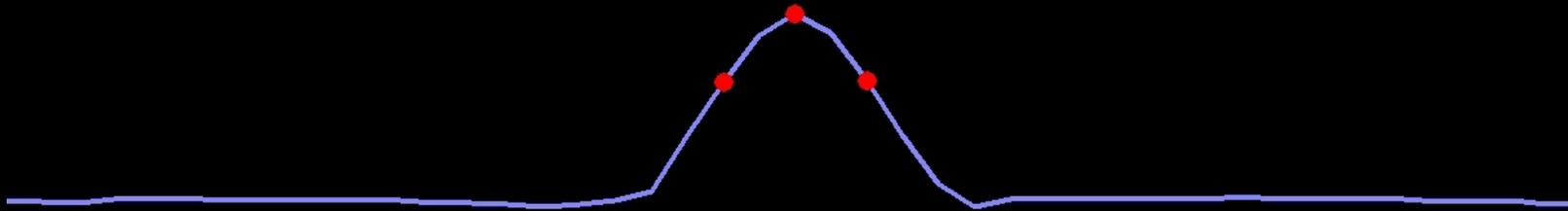
Direct-ascent ASAT could destroy individual satellites, but it would be impractical to take out full GPS constellation.

GNSS SPOOFING

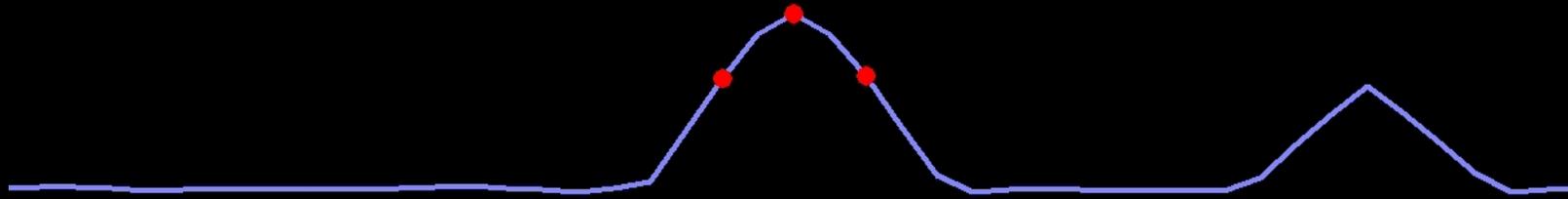
Spoofer mimics authentic GNSS satellites to hijack GNSS receiver tracking loops.



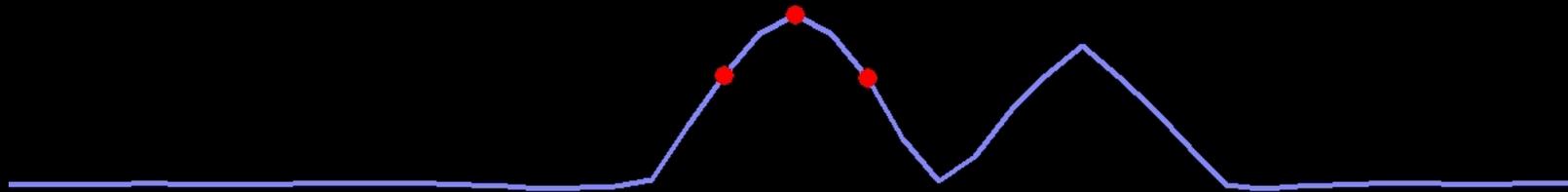
GPS Spoofer



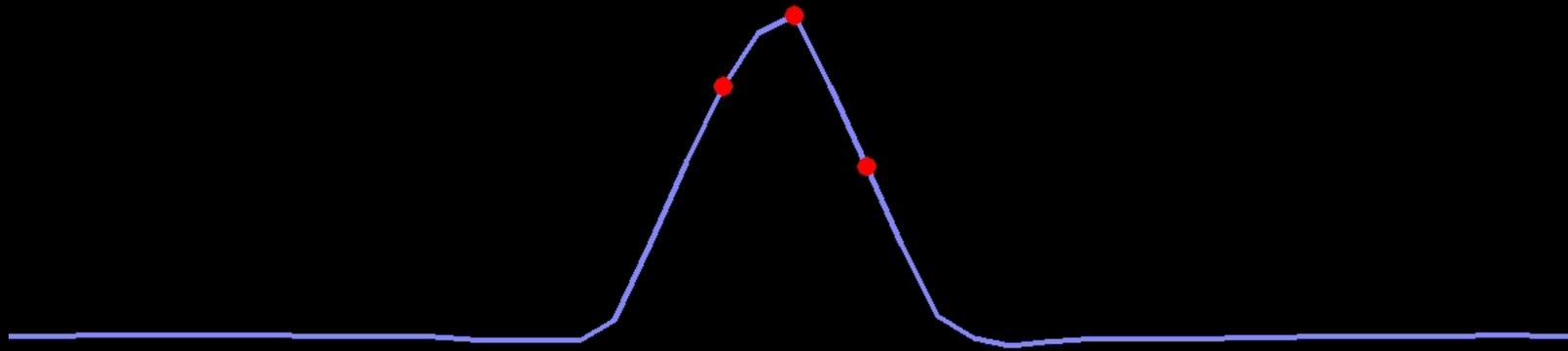
GPS Spoofer



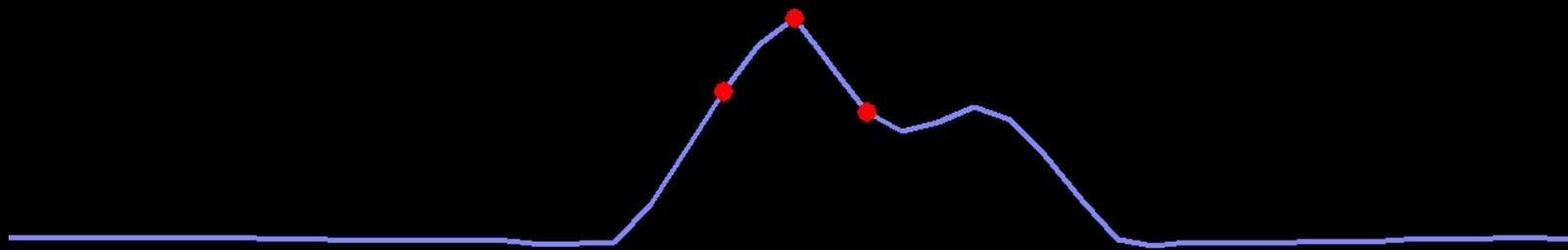
GPS Spoofer



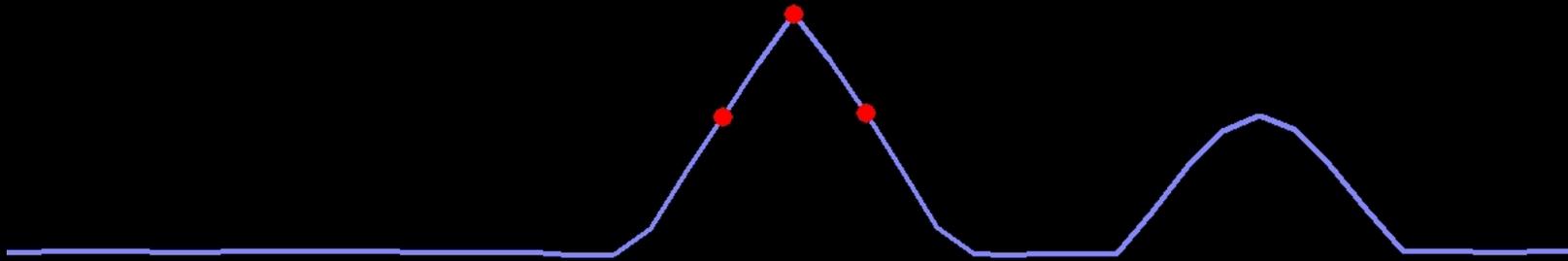
GPS Spoofer



GPS Spoofer



GPS Spoofer



Q: Is the GNSS spoofing vulnerability only theoretical, or has it been proven by experiment?

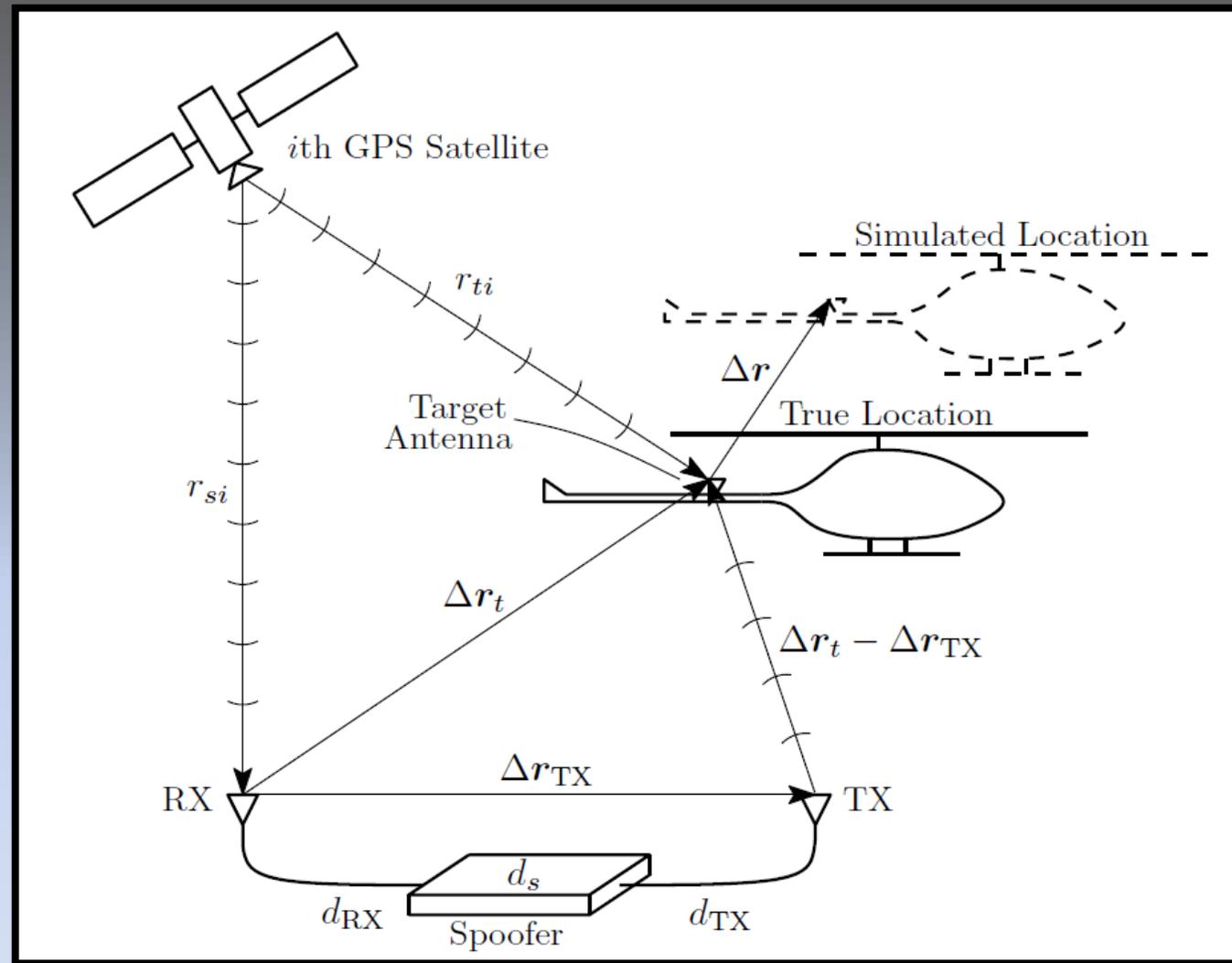
Building the
first publicly-
acknowledged
GPS spoofer,
2008



Humphreys, Todd E., et al. "Assessing the spoofing threat: Development of a portable GPS civilian spoofer." *Proceedings of the 21st International Technical Meeting of the Satellite Division of The Institute of Navigation (ION GNSS 2008)*. 2008.



First target: personal iPhone



Could false GNSS signals cause UAV to believe it's at the spoofer-simulated location, allowing full 3D hostile control of UAV?



\$60k Hornet Mini's navigation system sensors:
civil GNSS + baro + IMU + magnetometer

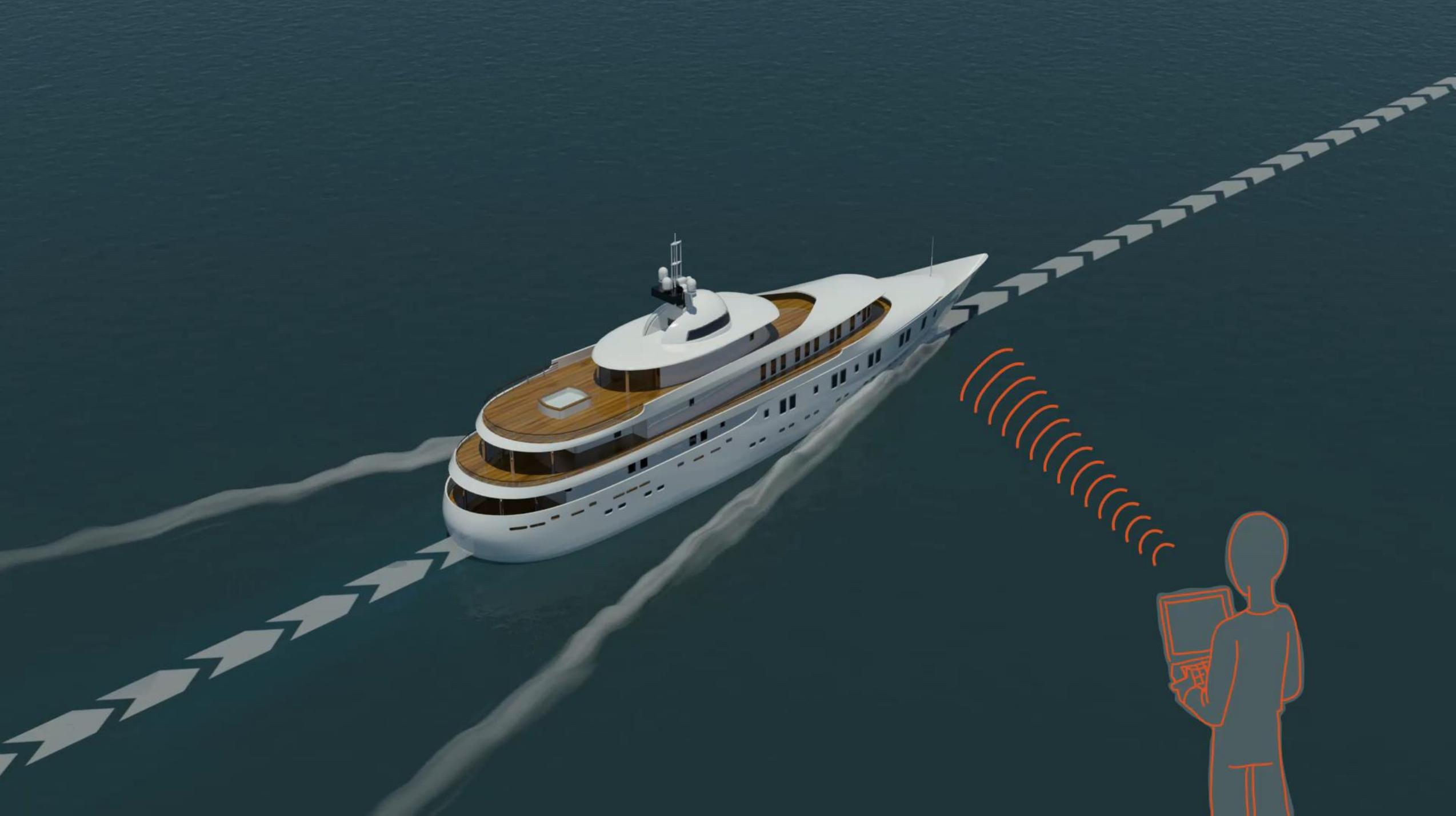


Kerns, Andrew J., Daniel P. Shepard, Jahshan A. Bhatti, and Todd E. Humphreys. "Unmanned aircraft capture and control via GPS spoofing." *Journal of Field Robotics* 31, no. 4 (2014): 617-636.



White Rose of Drachs: 65-meter, \$80M research laboratory in the Mediterranean





LMX 420 Navigation System

© POS 2

POSITION & TIME

Datum: W84

N 38°02.0768

E 22°48.1772

Altitude: -415.3m (3D)

Variation: 3.3° E

COG 126°

SOG 15.1Kn

Local time:

Saturday

29

June 2013

14:34:09

1
NAV
ABC

4
PLOT
JKL

7
POS
STU

E

Bhatti, Jahshan, and
Todd E. Humphreys.
"Hostile control of
ships via false GPS
signals: Demonstration
and detection."
*NAVIGATION, Journal
of the Institute of
Navigation* 64.1
(2017): 51-66.



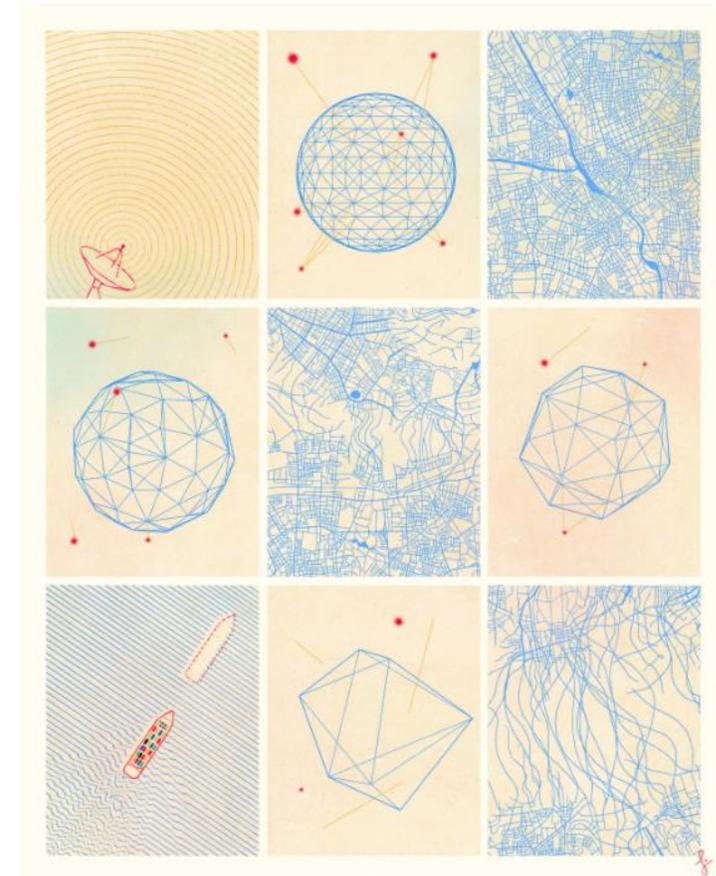
ANNALS OF TECHNOLOGY

HOW VULNERABLE IS G.P.S.?

*An engineering professor has proved—and exploited—its
vulnerabilities.*

By **Greg Milner**

August 6, 2020

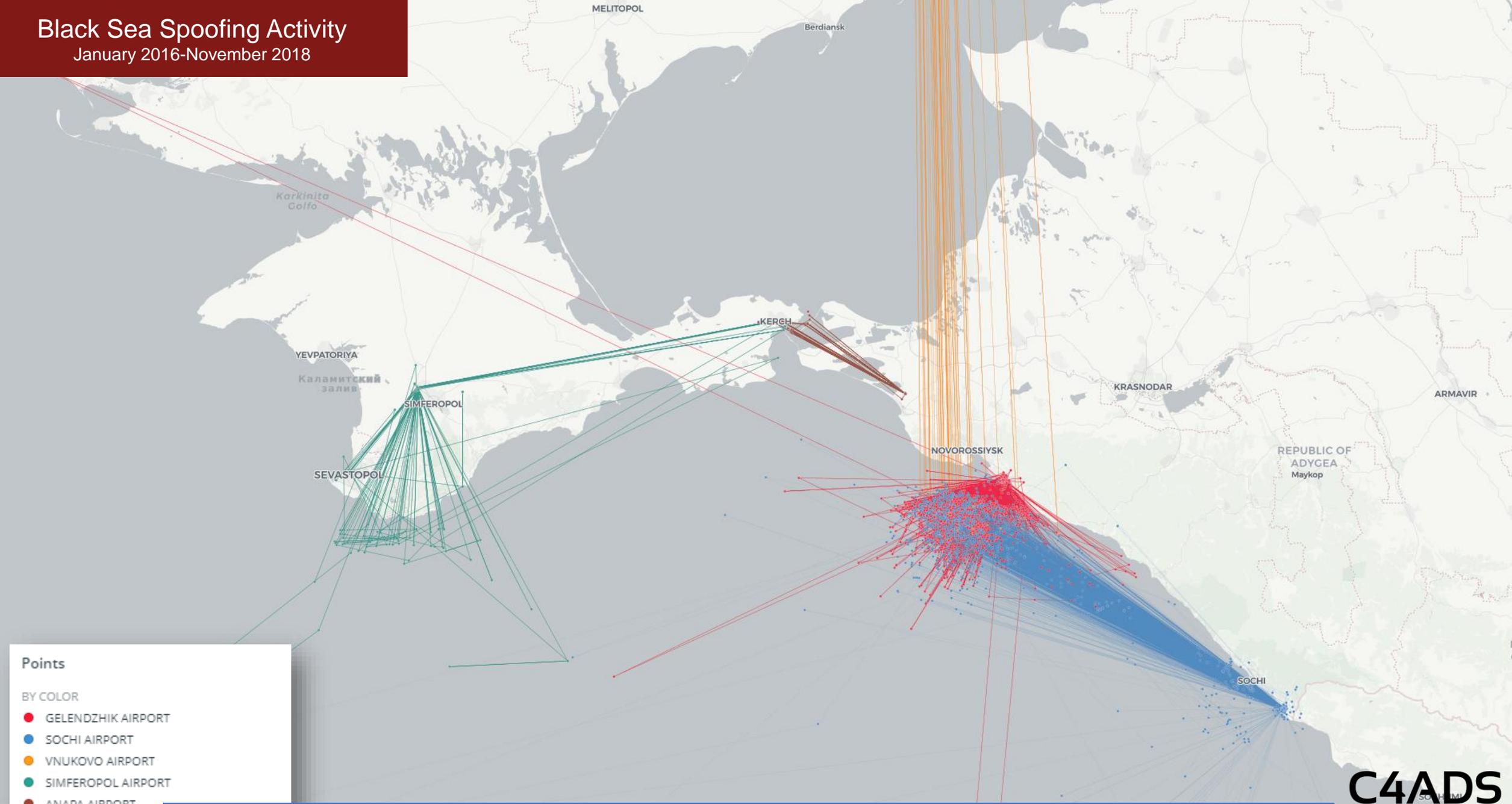


Profile of UT Radionavigation Lab's research in GNSS vulnerabilities
over past decade: *The New Yorker*, August 2020.

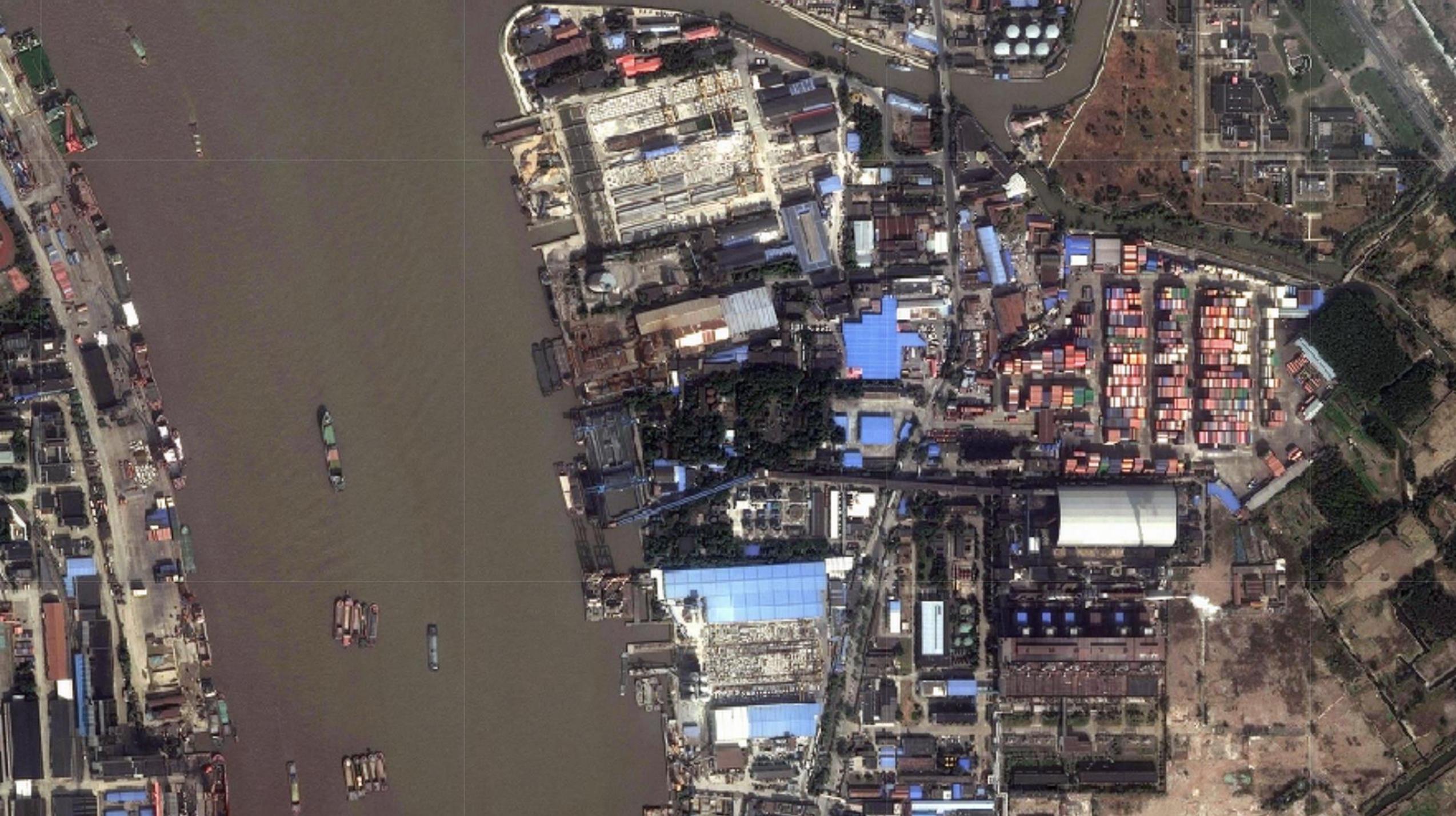
Q: Are GNSS vulnerabilities being exploited in the wild, or are they only laboratory phenomena?

Black Sea Spoofing Activity

January 2016-November 2018



C4ADS "Above Us Only Stars: Exposing GPS Spoofing in Russia and Syria."



Huangpu River

Dongtang Hwy

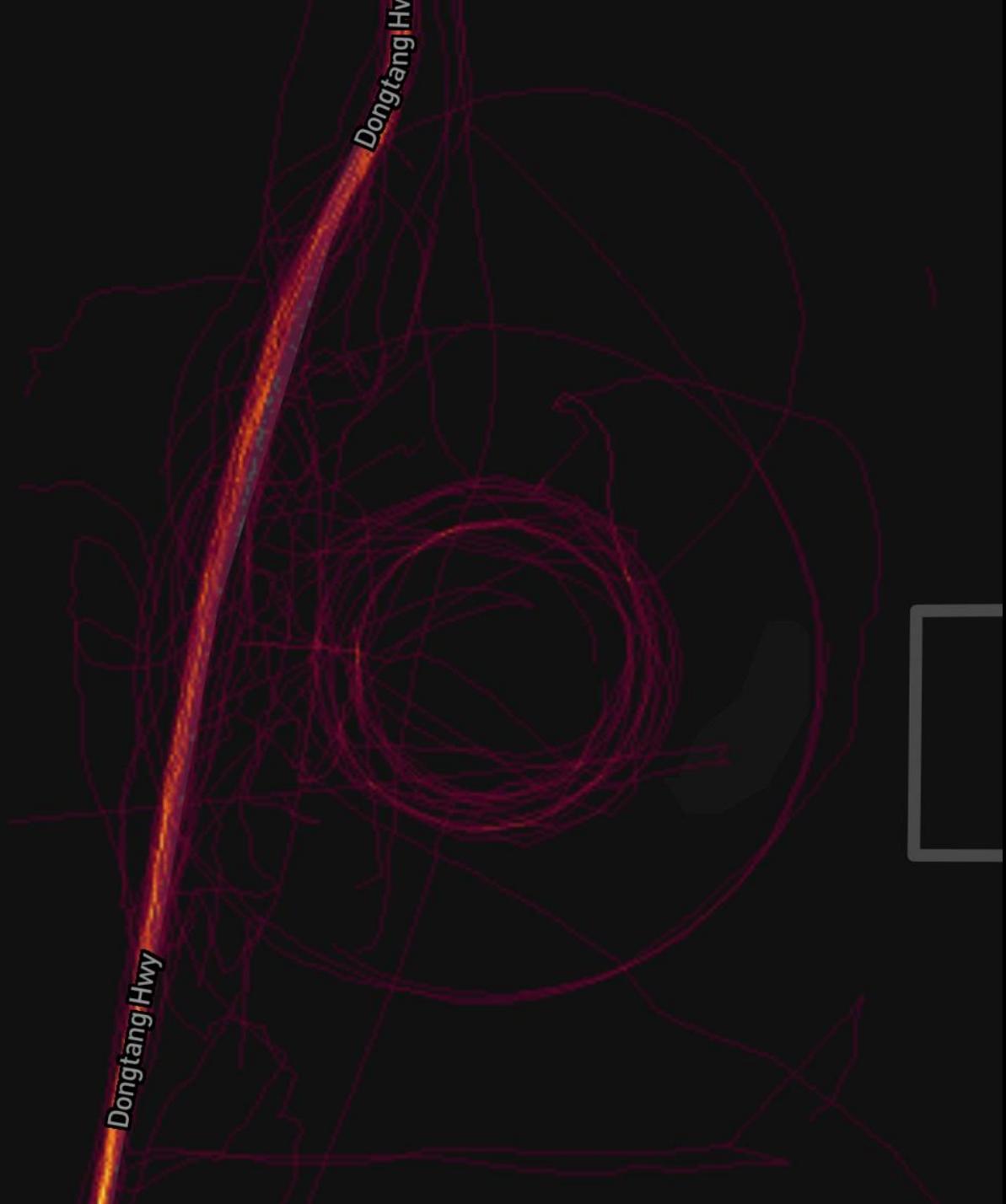
Hangnan Hwy

Ting'an Rd

Zhouhai Rd

Qi Fan Road





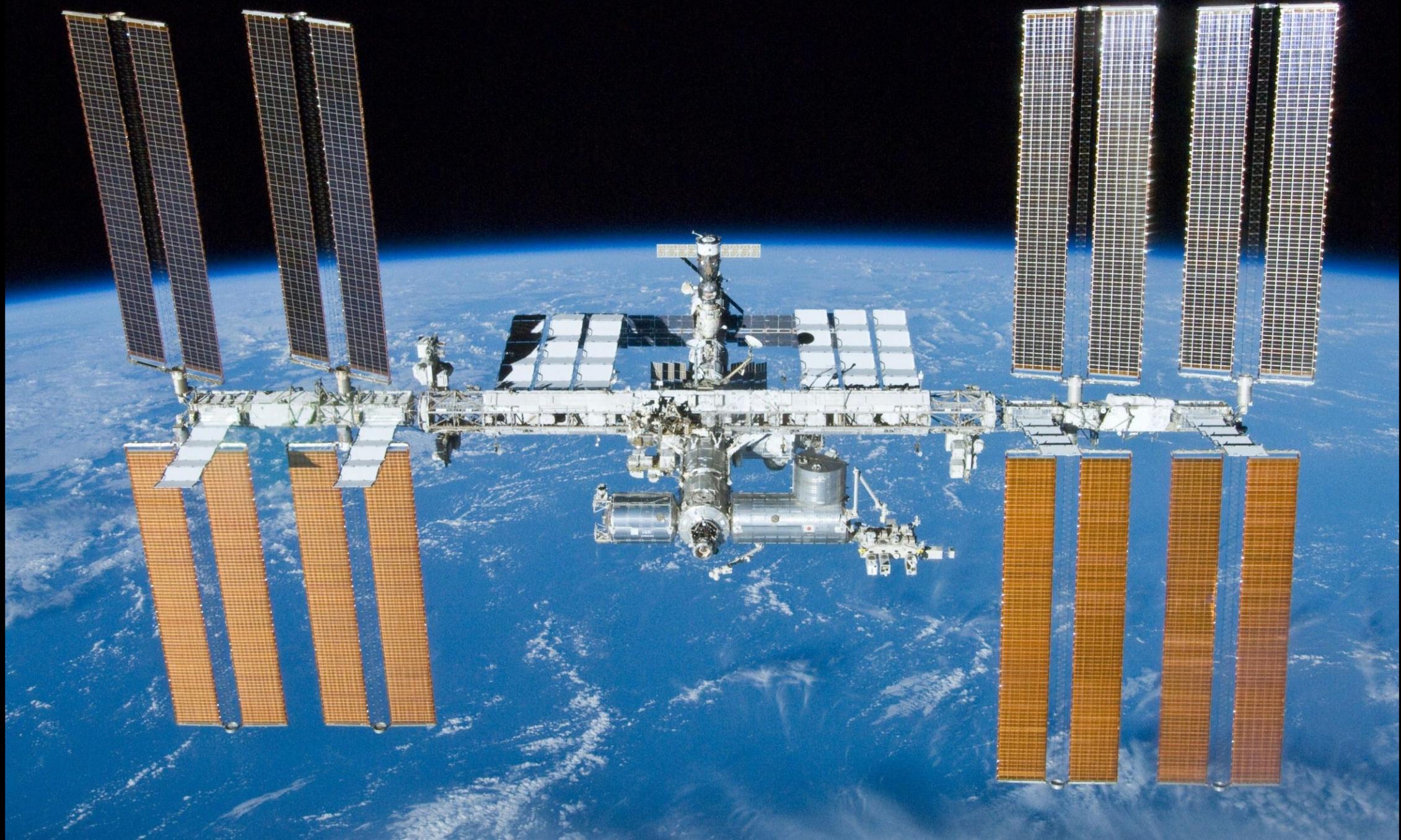


Capable turnkey GNSS spoofer can now be purchased for less than \$300

Q: Can LEO SVs be used for global GNSS interference monitoring?



A flexible, science-grade GNSS receiver in low-earth orbit (LEO) would enable continuous global monitoring and characterization of GNSS interference





February 2017: FOTON SDR installed on International Space Station

Science mission: Ionospheric sensing via radio occultation and airglow meas.

Collaborators: Naval Research Lab, Cornell, University of Texas, Aerospace Corp.



GPS

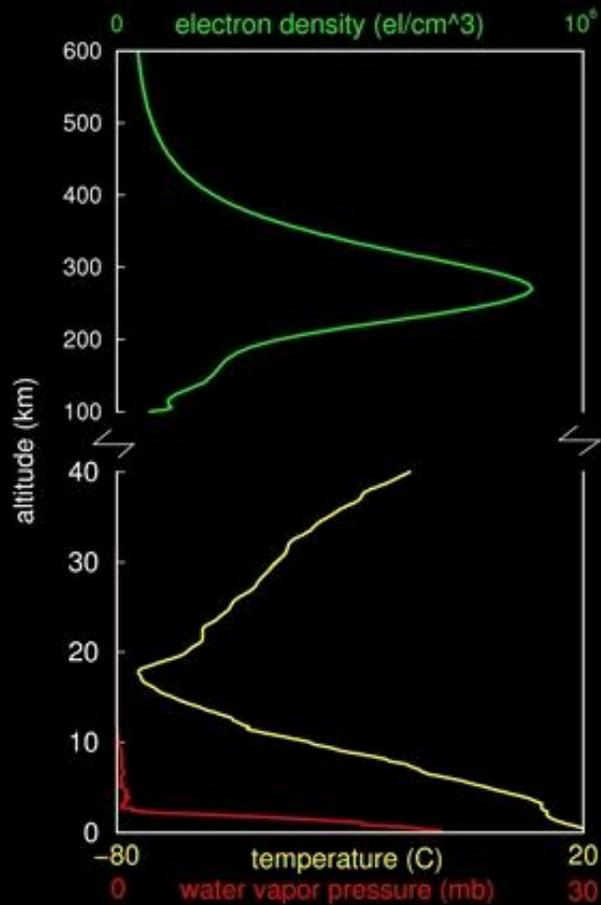
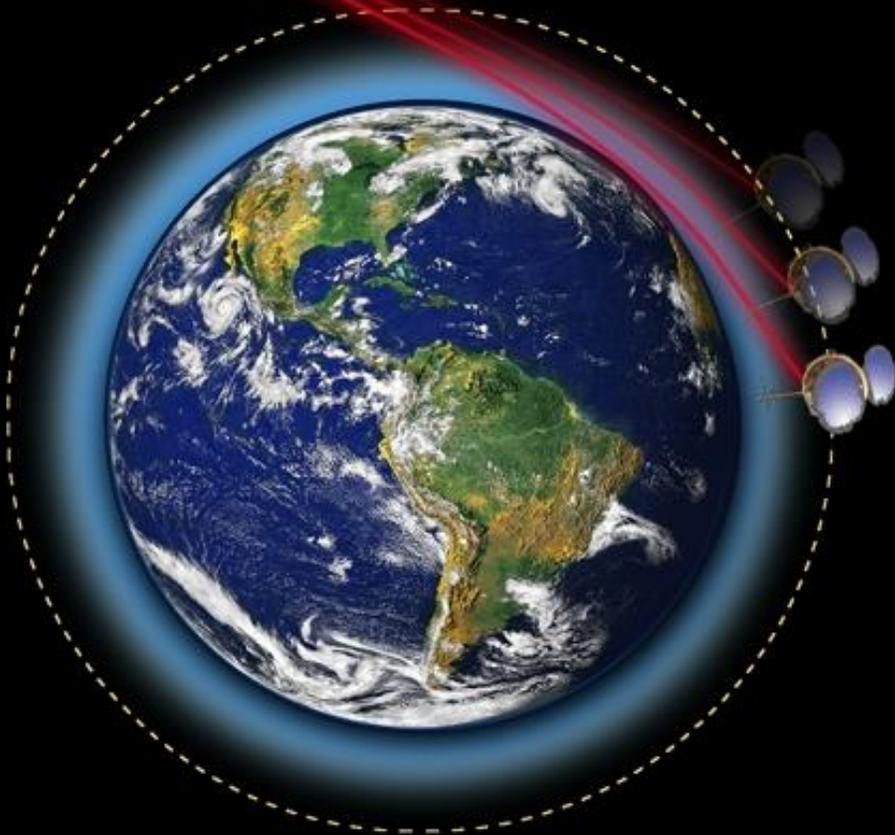


Image: UCAR COSMIC Program

Black Sea Spoofing Activity

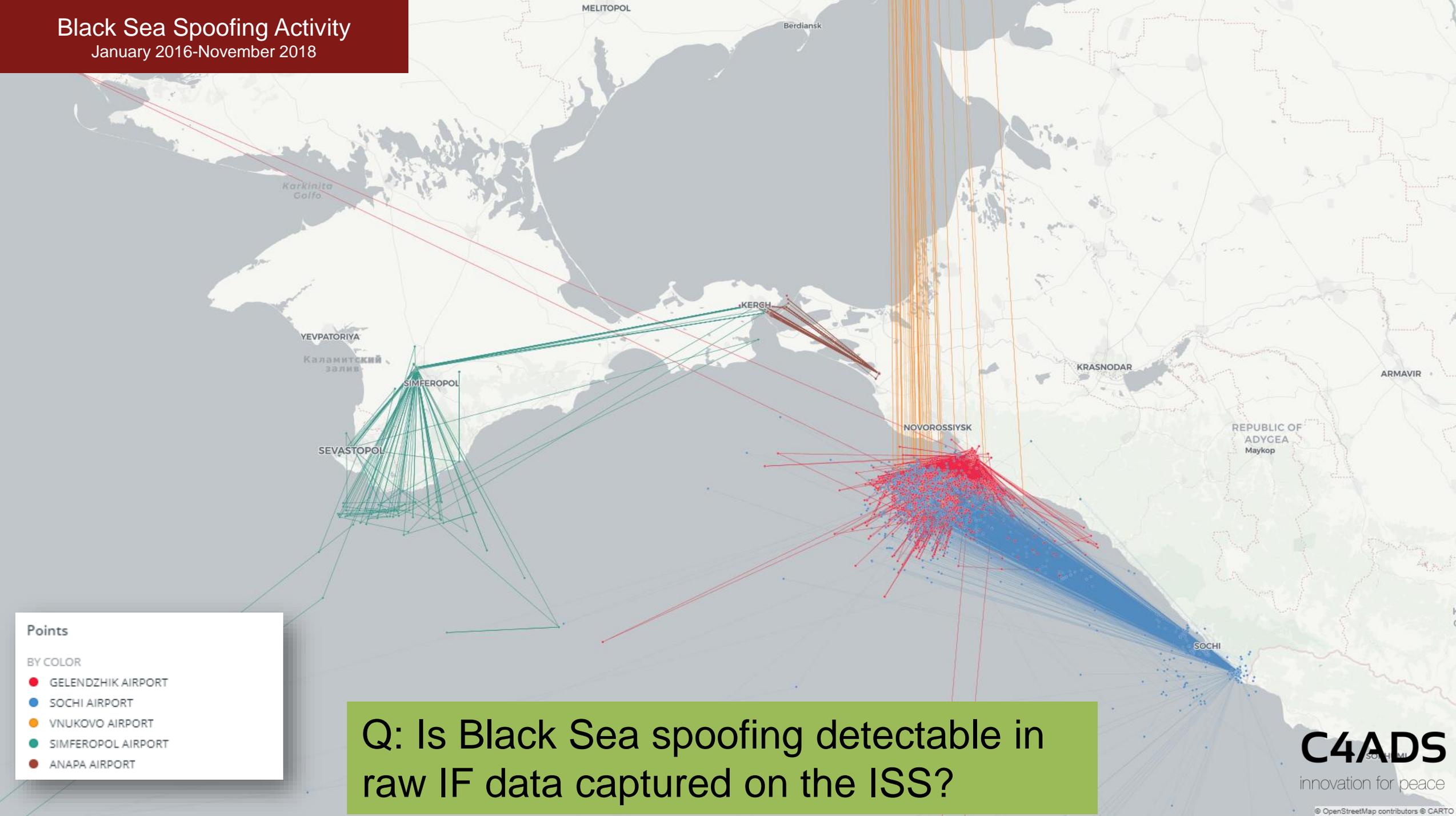
January 2016-November 2018

Points

BY COLOR

- GELENDZHIC AIRPORT
- SOCHI AIRPORT
- VNUKOVO AIRPORT
- SIMFEROPOL AIRPORT
- ANAPA AIRPORT

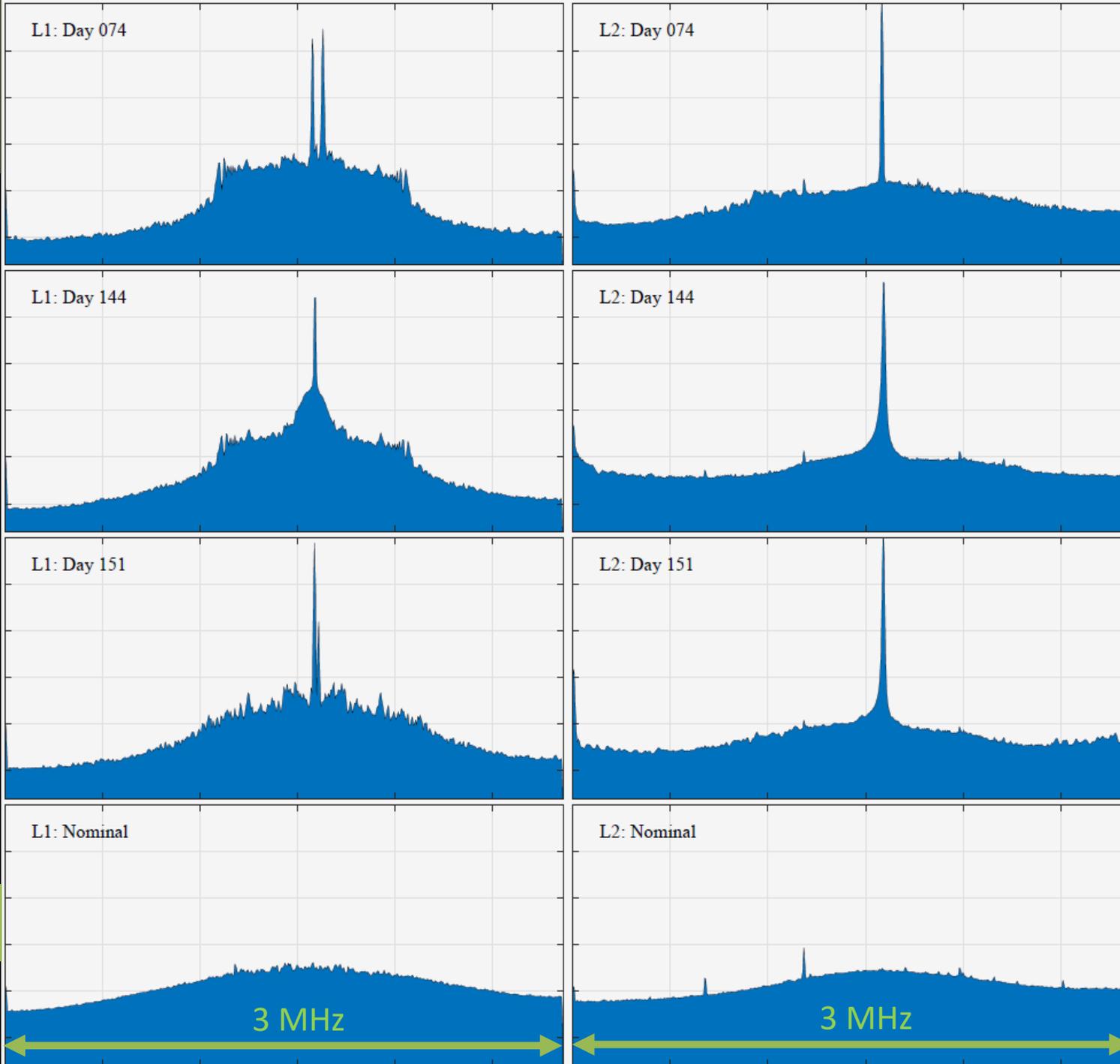
Q: Is Black Sea spoofing detectable in raw IF data captured on the ISS?





March-May 2018: Raw IF samples captured near Black Sea on 3 separate days
60-second recordings sent via NASA's communications backbone to NRL and thence to UT for processing with latest version of GRID

Power Spectra



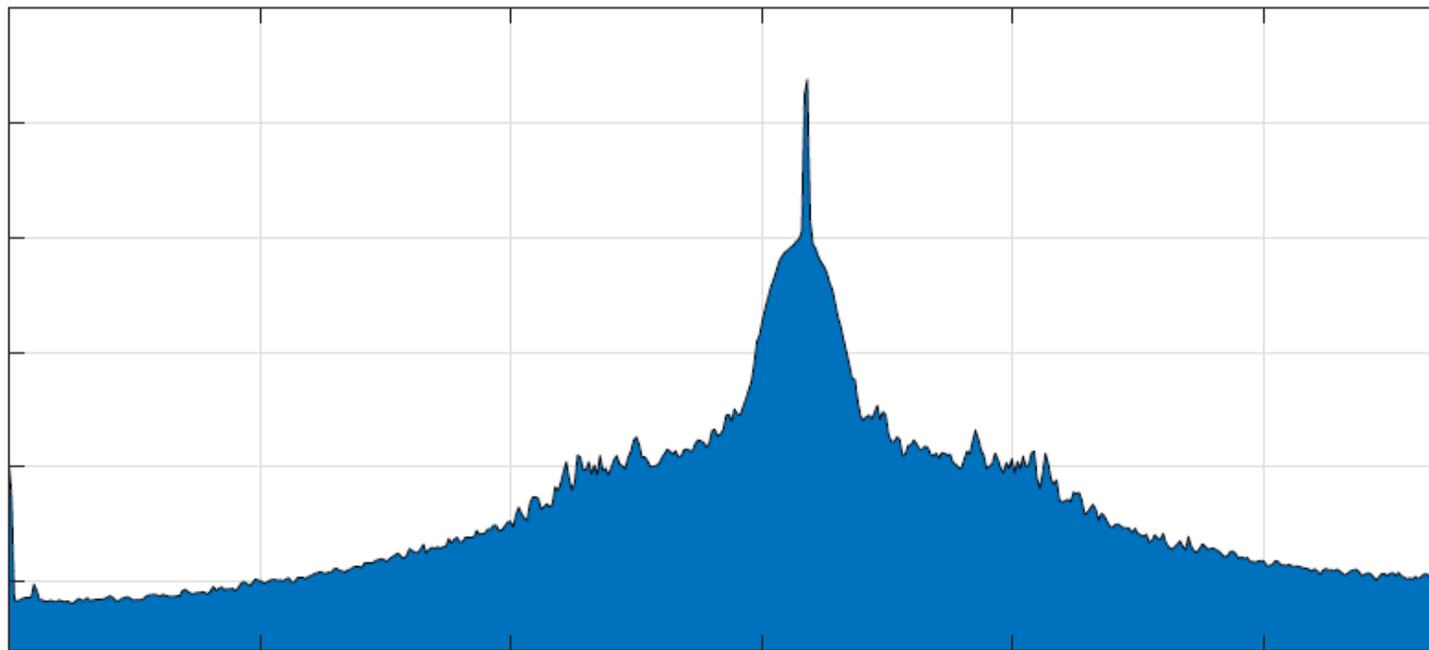
L1: 1575.42 MHz

L2: 1227.6 MHz

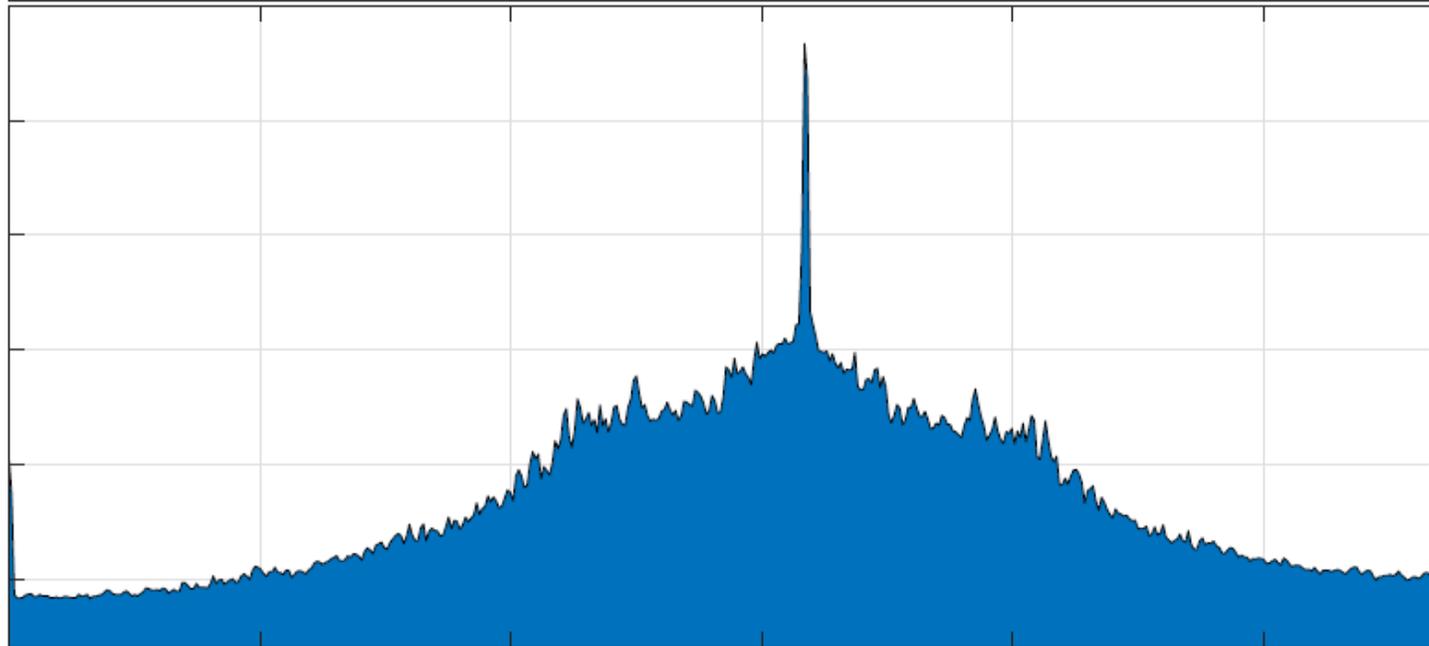
3 MHz

3 MHz

Maximum



Minimum



250 kHz rounded prominence at L1 waxes and wanes with an approximately 5 sec. period

GPS L1 CA PRIMARY

1	19u	-29228.2	-0.0	0.0	39.3	359.4	-75.1	5*
2	5u	-29228.2	-0.0	0.0	40.2	54.9	-38.4	5*
3	12u	-29228.7	-0.0	0.0	41.3	107.6	-47.8	5*
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8	16	-40379.6	2650169.5	21204591.2	40.5	220.0	10.2	6
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12	8	-10484.9	76068.5	20159639.2	32.0	311.3	29.4	6
13	10	-7468.0	328301.5	17415104.7	38.9	227.7	79.1	6

“Coded” jamming via authentic spreading codes

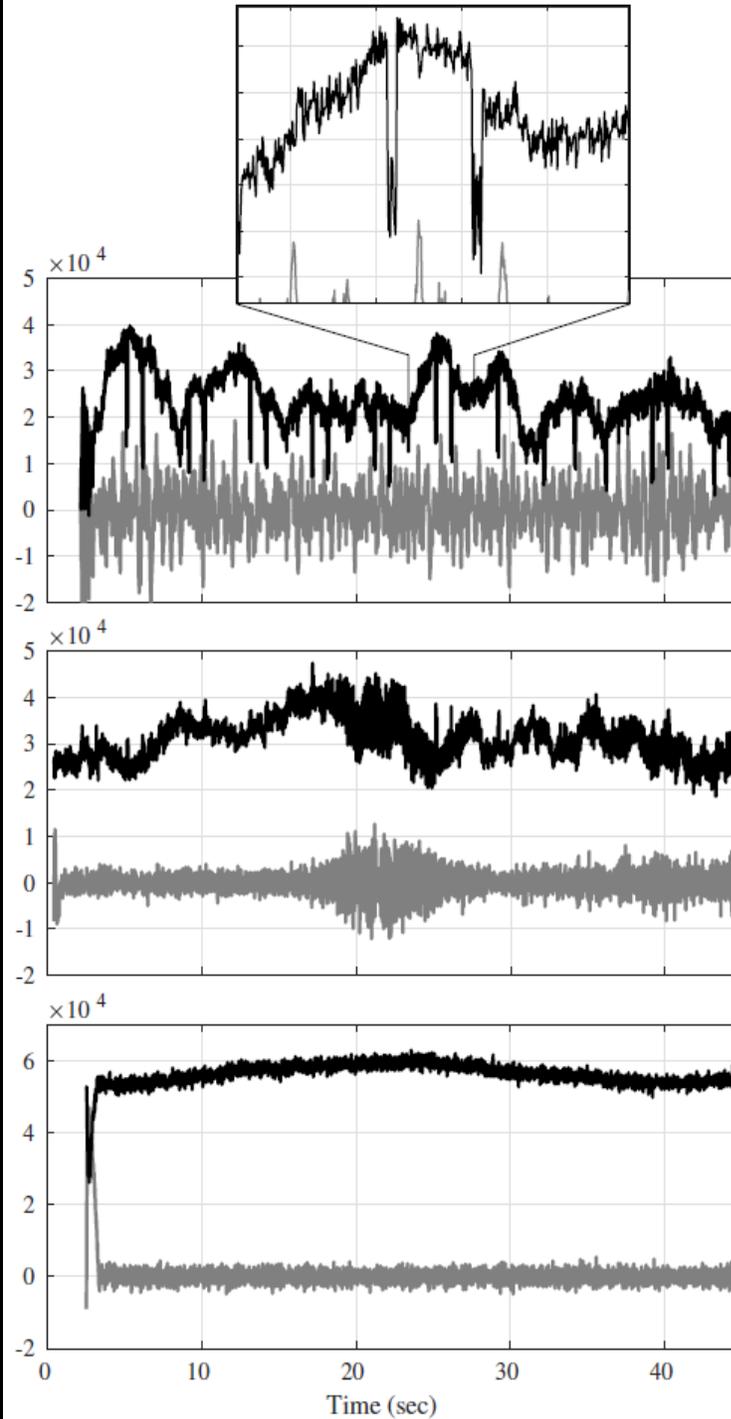
The Syrian interference source employs *coded jamming*. Its purpose appears to be denial of GPS service, but it achieves this by *spoofing* each of the GPS L1 C/A PRN codes (albeit without LNAV modulation).

Data-Wiped 100-Hz IQ accumulations

False signal

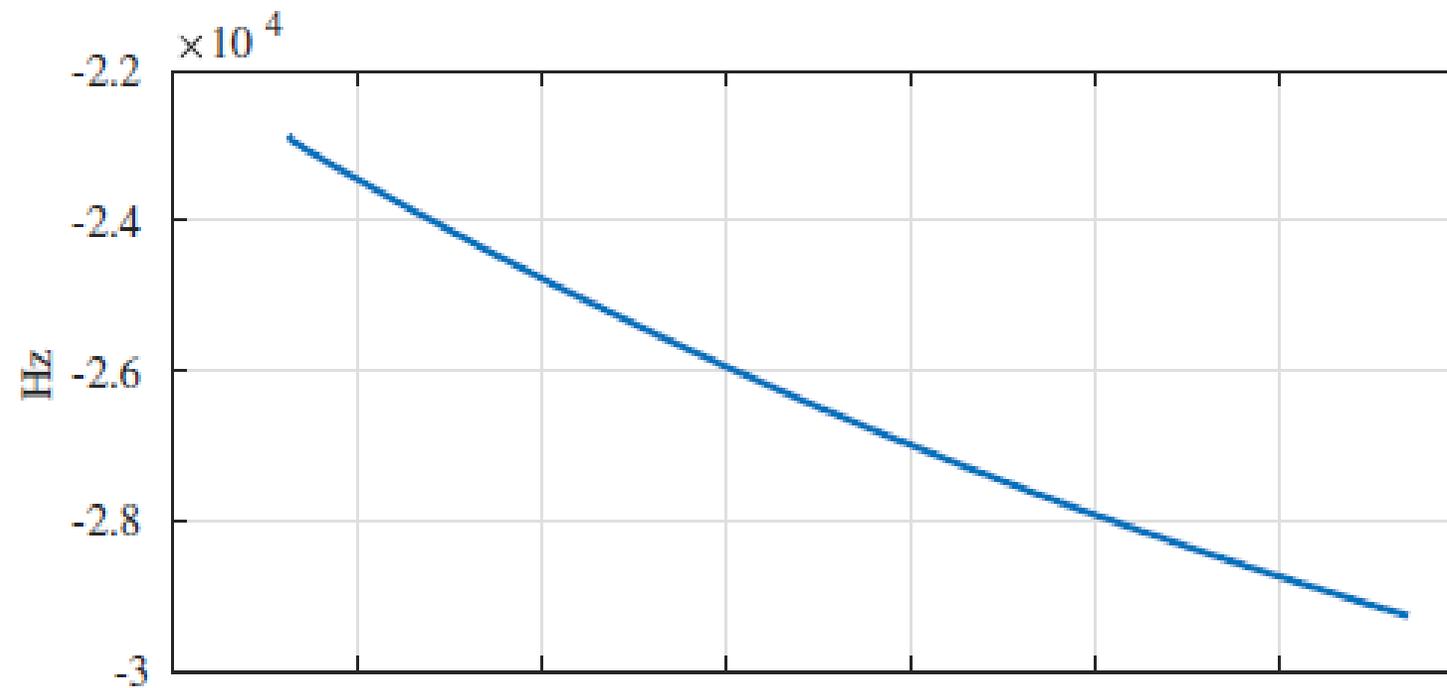
Authentic signal
in interference

Authentic signal
under clean
conditions



Unexplained
fading

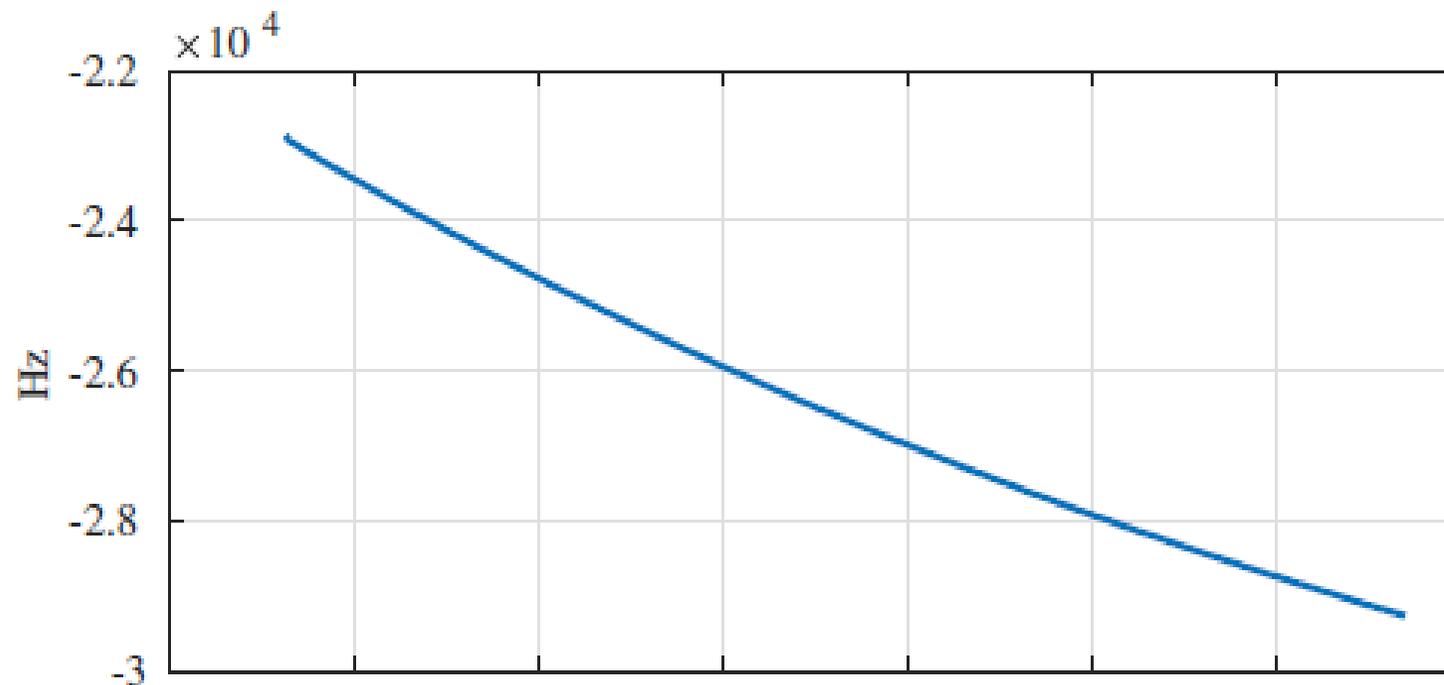
Doppler time history
for false PRN 10 signal
from day 144 capture



Doppler model
nonlinearly related to
transmitter position,
but also strongly
affected by transmitter
clock error rate.

$$f_D = -\hat{\mathbf{r}}^T \mathbf{v}_R / \lambda - c \left[\delta \dot{t}_R - \delta \dot{t}_T (1 - \delta \dot{t}_R) \right] / \lambda + w$$

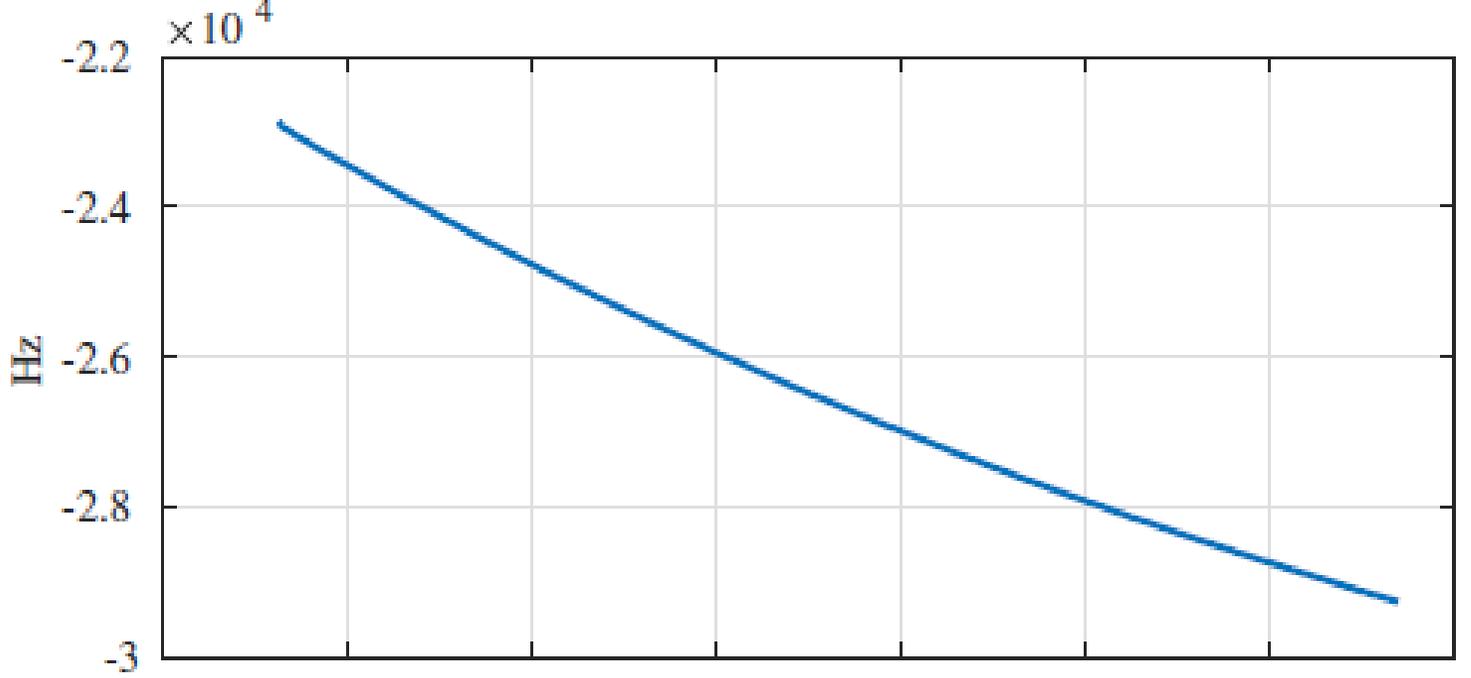
Doppler time history
for false PRN 10 signal
from day 144 capture



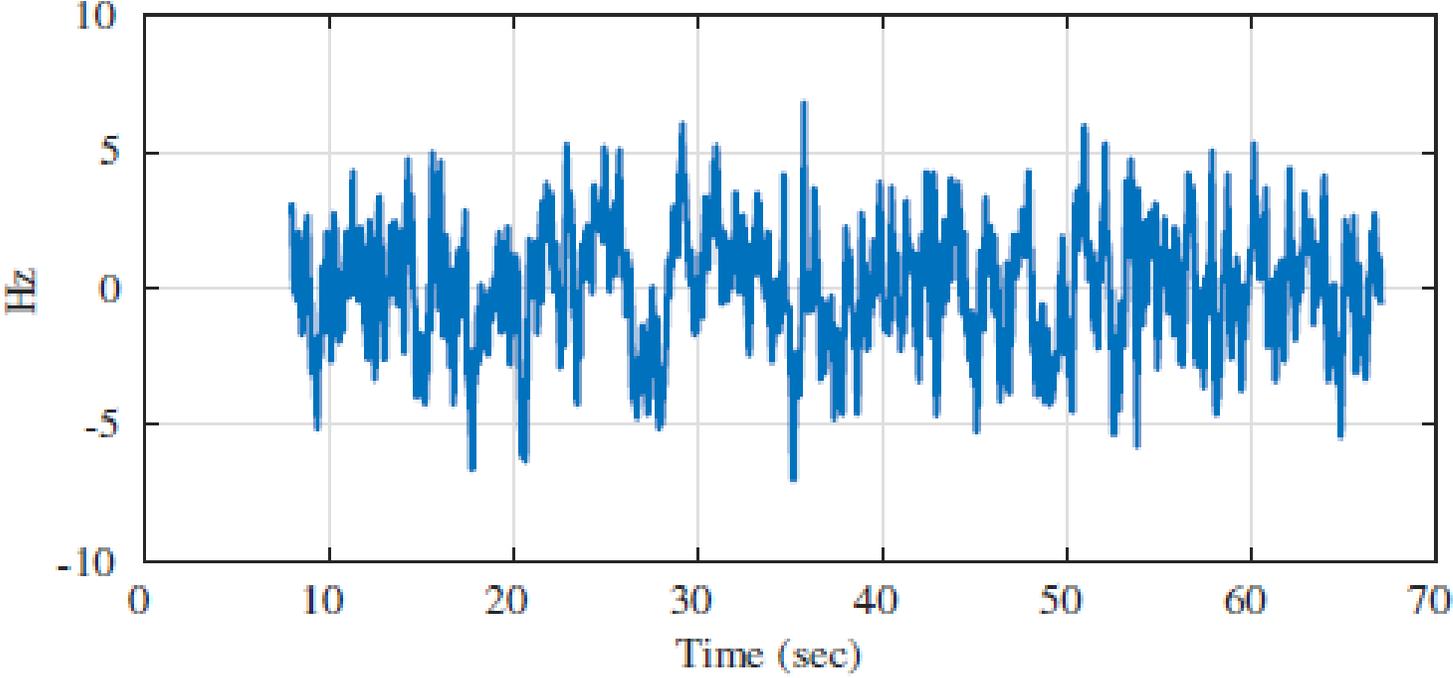
Marginal
contribution of TX
frequency instability
to a single-pass
geolocation error
ellipse semi major
(a) and semi minor
(b) axes

Clock Quality	h_{-2}	a (m)	b (m)
TCXO	3×10^{-21}	6900	690
Low-quality OCXO	3×10^{-23}	720	72
OCXO	3×10^{-25}	67	7.4

Doppler time history
for false PRN 10 signal
from day 144 capture



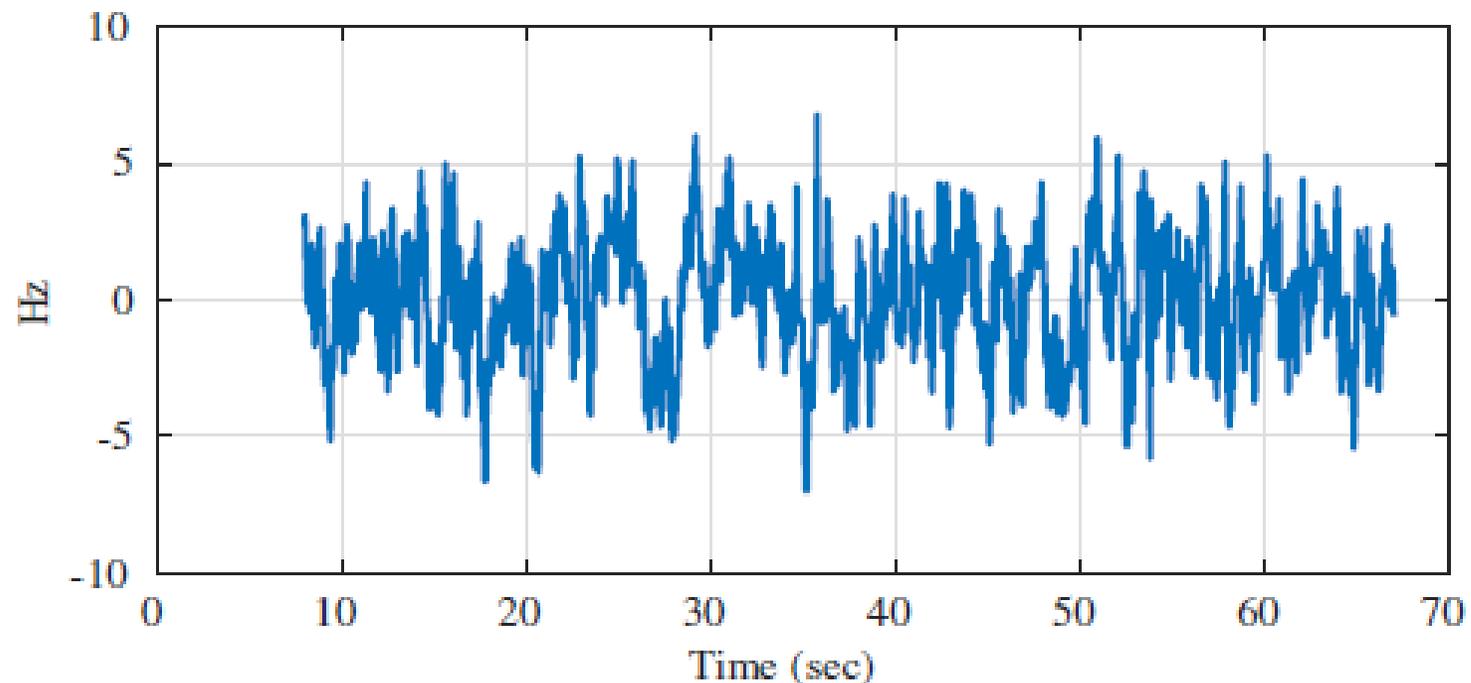
Post-fit residuals of
Doppler time history
assuming estimated
transmitter location
and clock rate offset

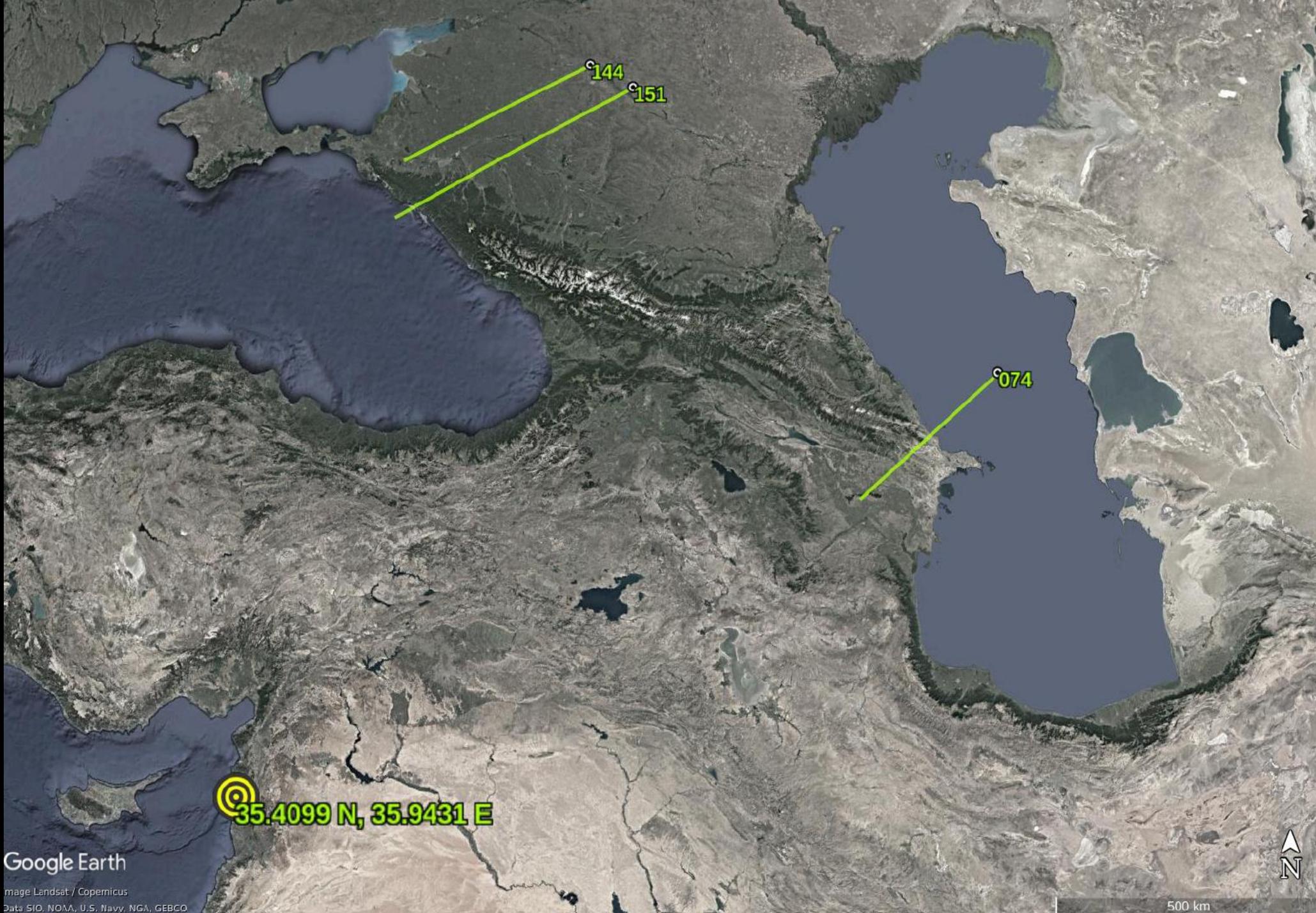


Analysis of the estimated clock frequency rate for days 74 and 144 revealed an Allan deviation consistent with an OCXO

$$\sigma_y(2, \tau, \tau) = 1.6 \times 10^{-11}$$

Post-fit residuals of Doppler time history assuming estimated transmitter location and clock rate offset





144

151

074



35.4099 N, 35.9431 E

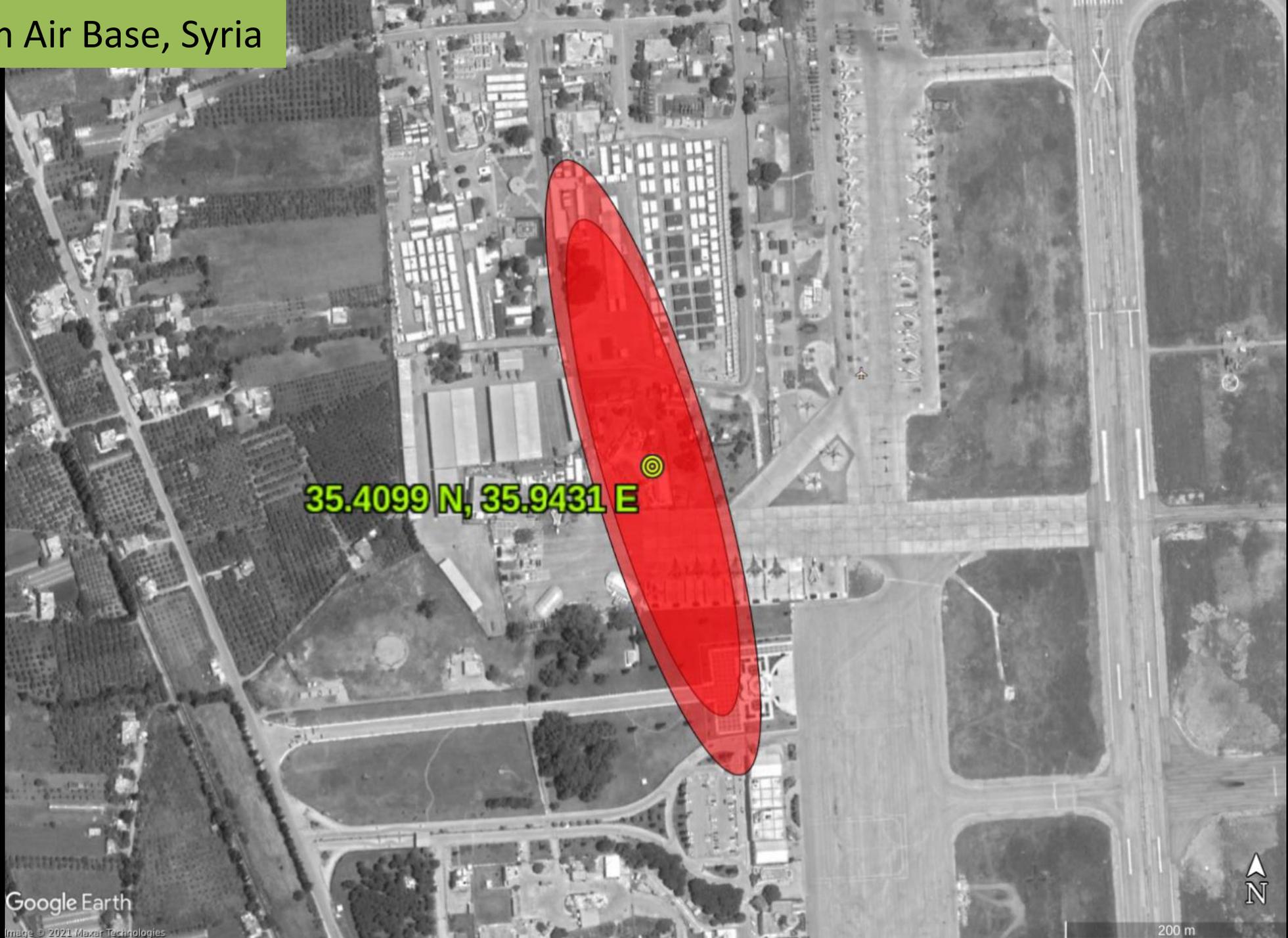
Google Earth

Image Landsat / Copernicus
Data SIO, NOAA, U.S. Navy, NGA, GEBCO

500 km



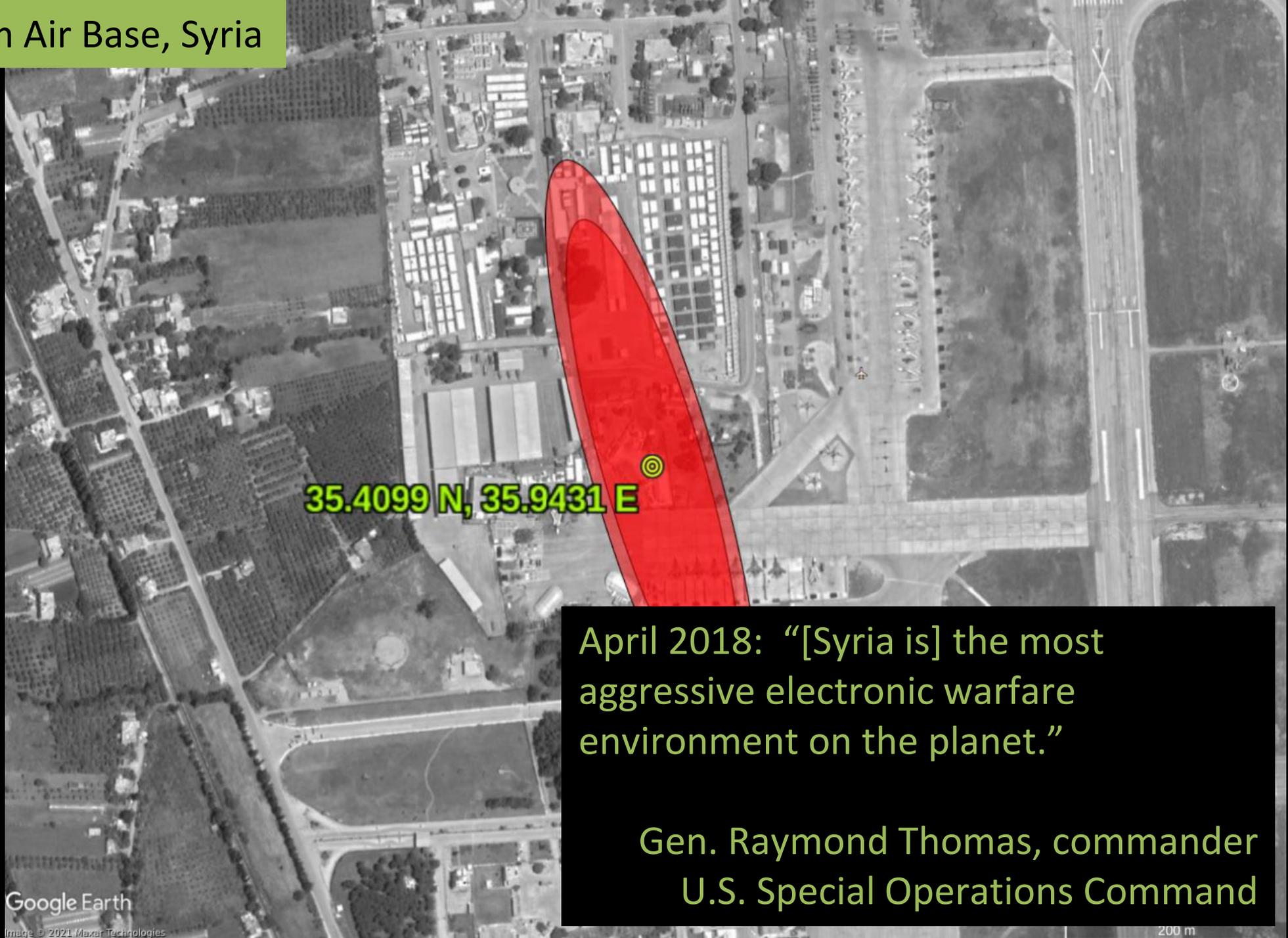
Khmeimim Air Base, Syria



35.4099 N, 35.9431 E



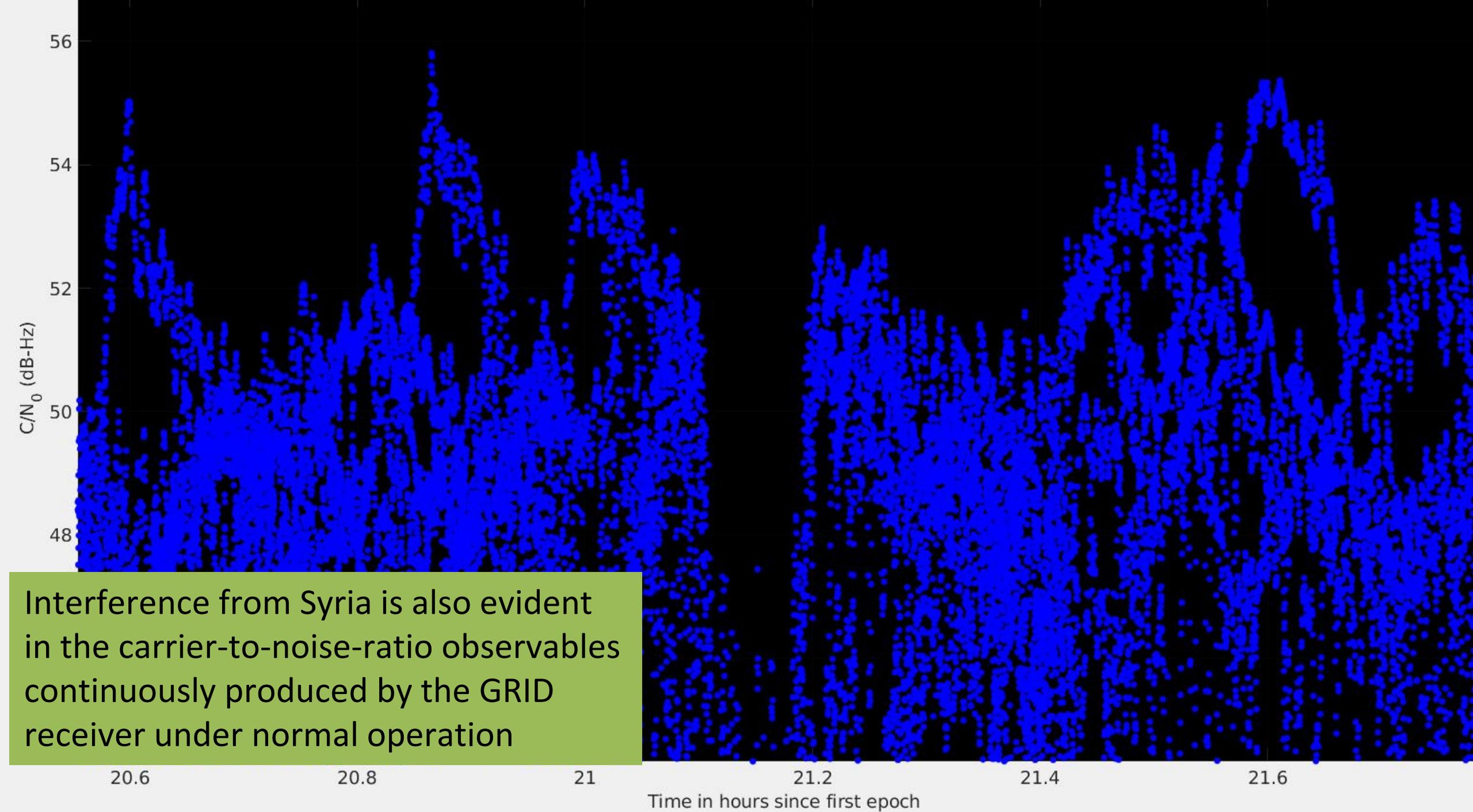
Khmeimim Air Base, Syria



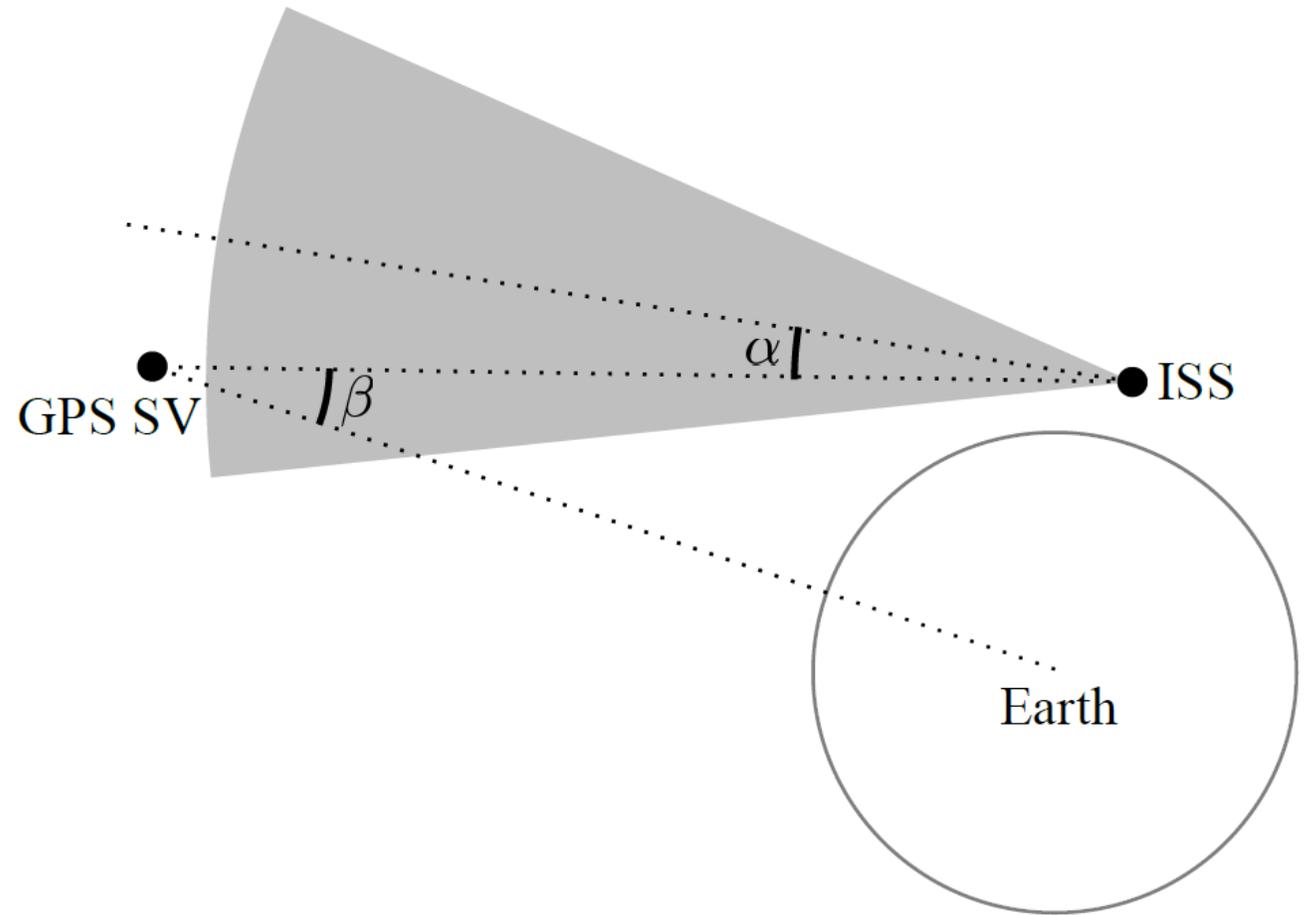
35.4099 N, 35.9431 E

April 2018: “[Syria is] the most aggressive electronic warfare environment on the planet.”

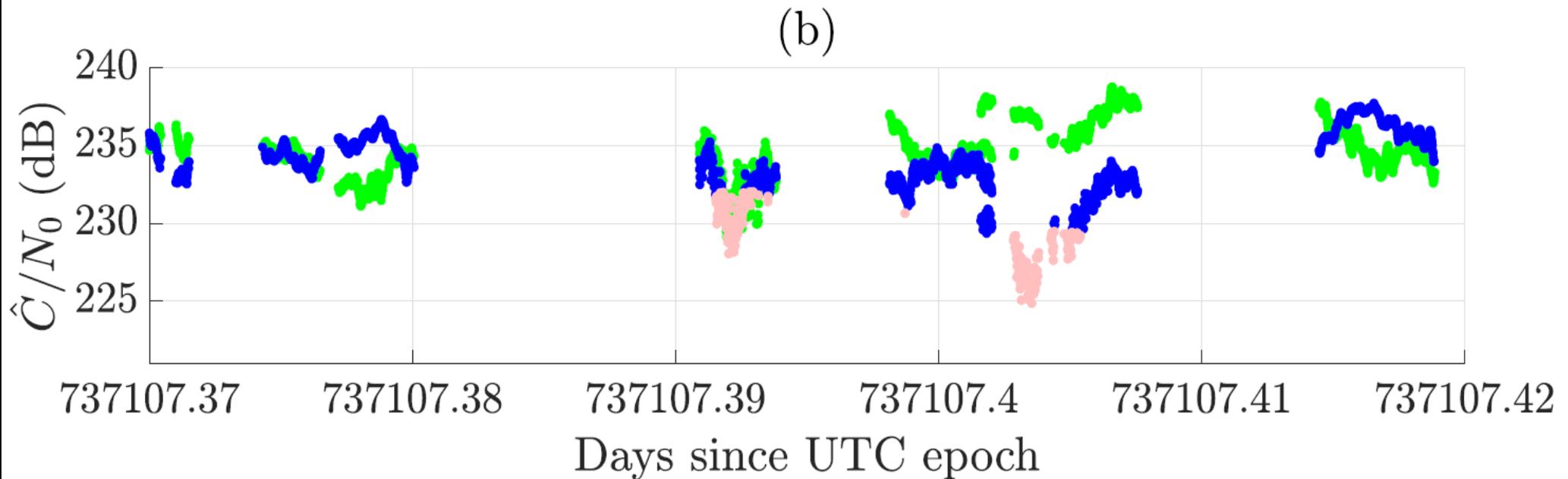
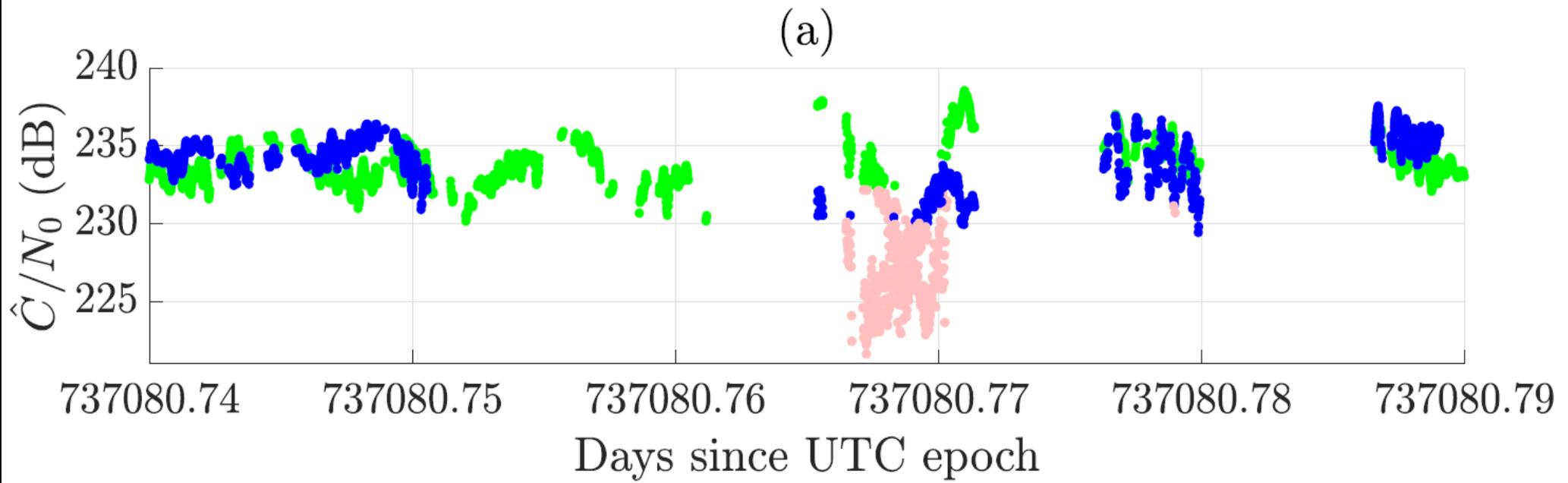
Gen. Raymond Thomas, commander
U.S. Special Operations Command



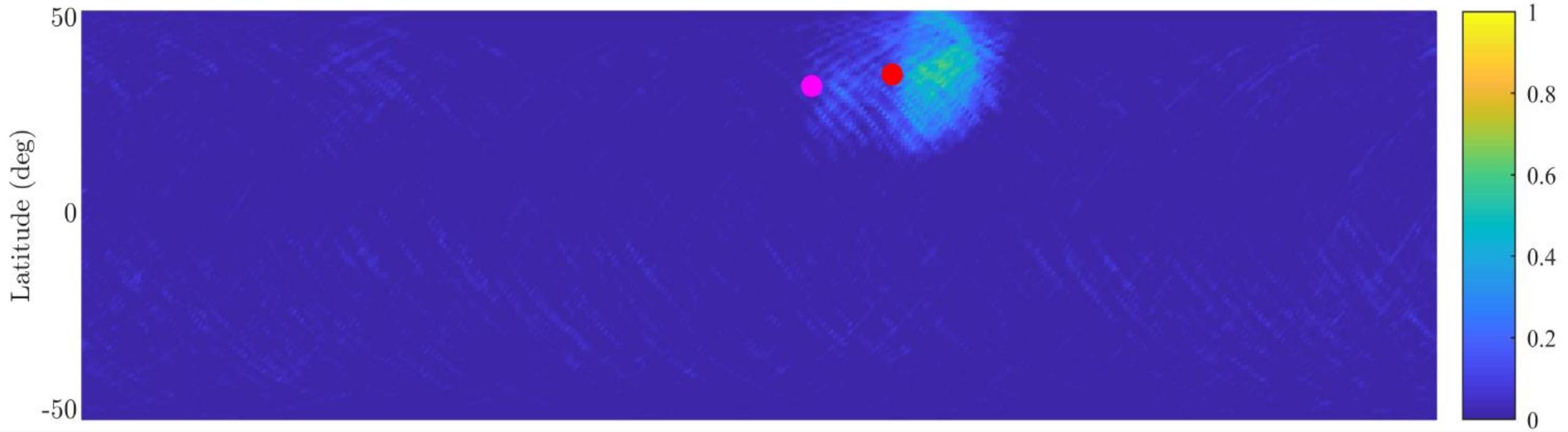
$$C(j, f, r_{sr}, z_s, z_r)$$



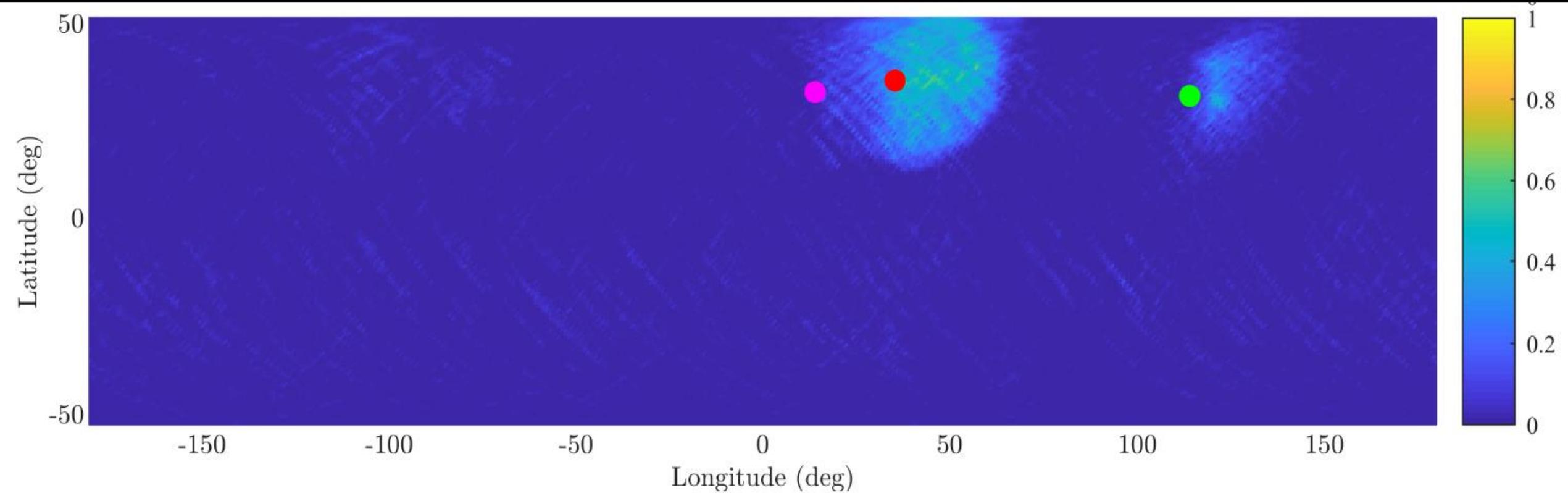
To maximize detectability, CINR observations must be pre-processed to compensate for predictable variations due to PRN (j), frequency (f), range (r_{sr}), satellite off-boresight angle (z_s), and receiver off-boresight angle (z_r).



Model-compensated receiver-reported CINR as ISS overflies interference zones



Heat map based on standard 1-Hz L1 C/N0 data from ISS GRID receiver from March 2017 to June 2020. The interference source in Syria is clearly evident, with a pattern asymmetry due to the receiver's antenna pointing aft. A second source near Libya is also evident.



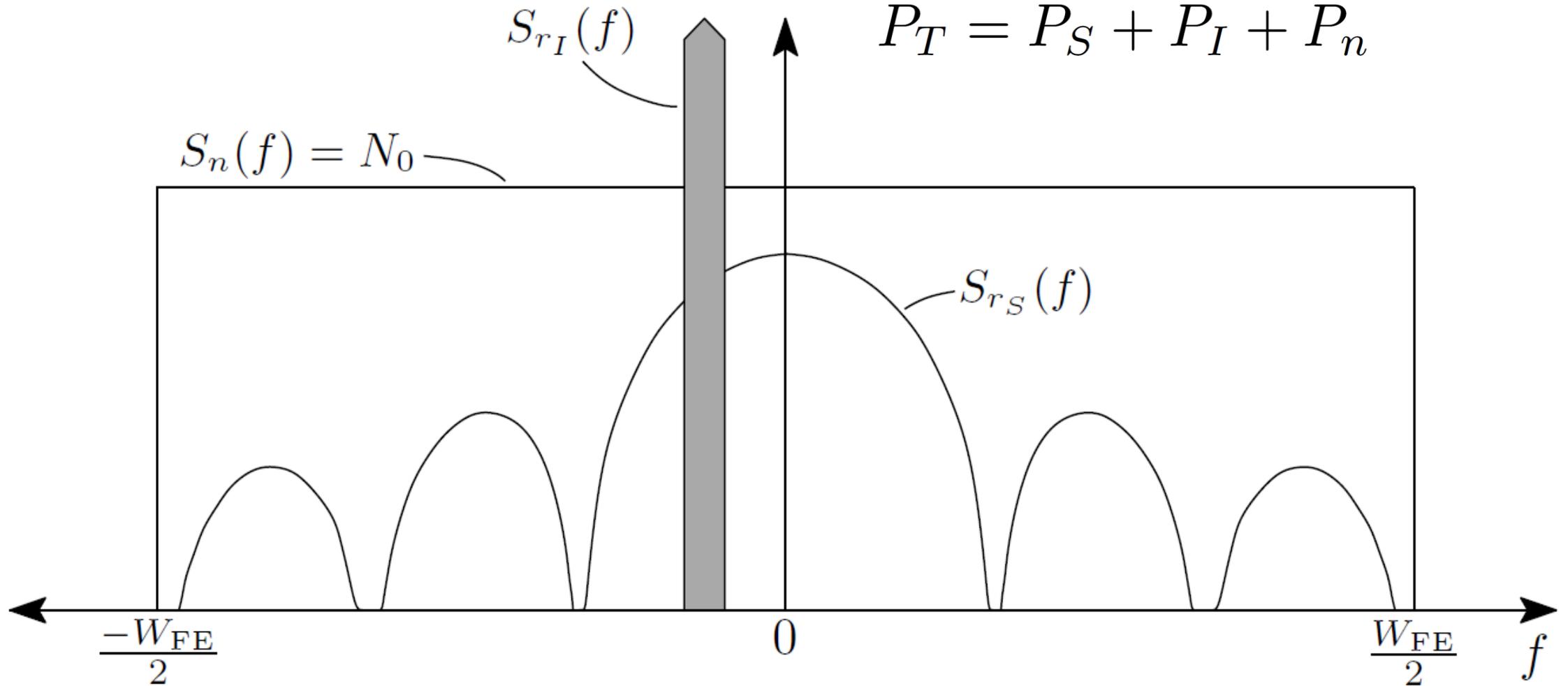
Heat map based on standard 1-Hz L2 C/N0 data from ISS GRID receiver from March 2017 to June 2020. Interference from Syria is evident, as is a persistent signature in mainland China at approximately 32 N, 114 E.

M. J. Murrian, L. Narula, P. A. Iannucci, S. Budzien, B. W. O'Hanlon, S. P. Powell, and T. E. Humphreys, "First results from three years of GNSS interference monitoring from low Earth orbit," *Navigation, Journal of the Institute of Navigation*, 2021. Submitted for review.

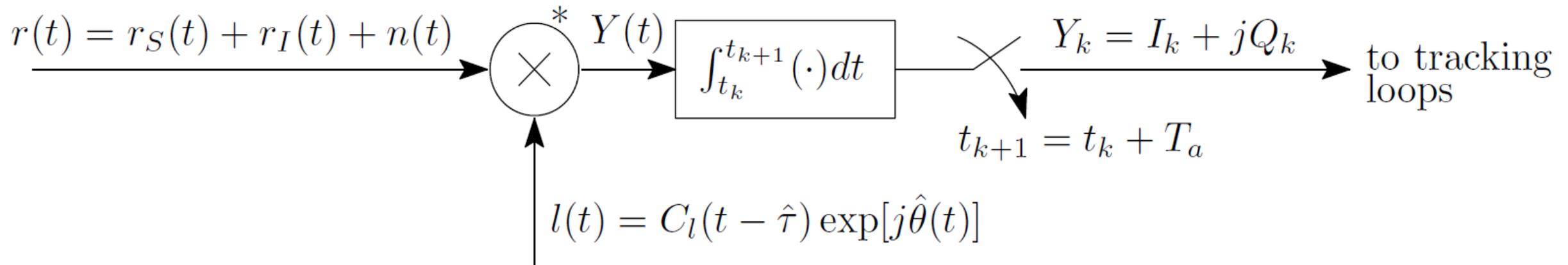
Q: How does one calculate the effect of a given interference waveform on an GNSS receiver?

$$r(t) = r_S(t) + r_I(t) + n(t)$$

$$P_T = P_S + P_I + P_n$$



Received signal is a mixture of signal, interference, and noise

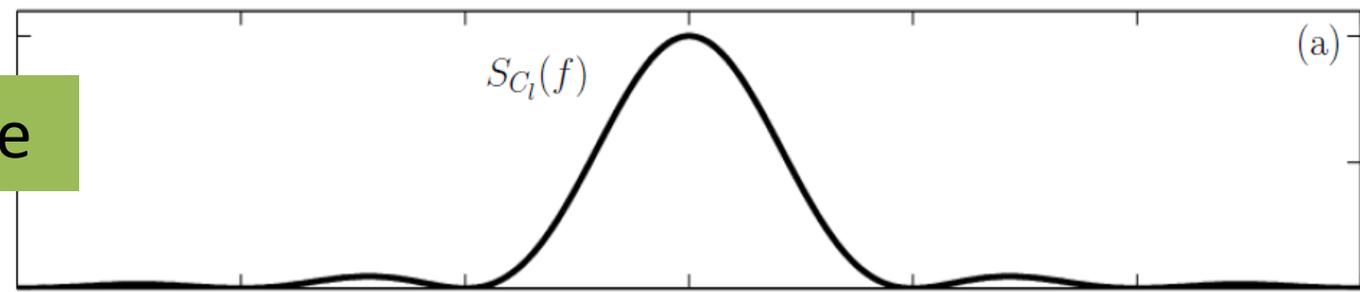


$$I(t) = r_I^*(t) C_l(t - \hat{\tau}) \exp[j\hat{\theta}(t)]$$

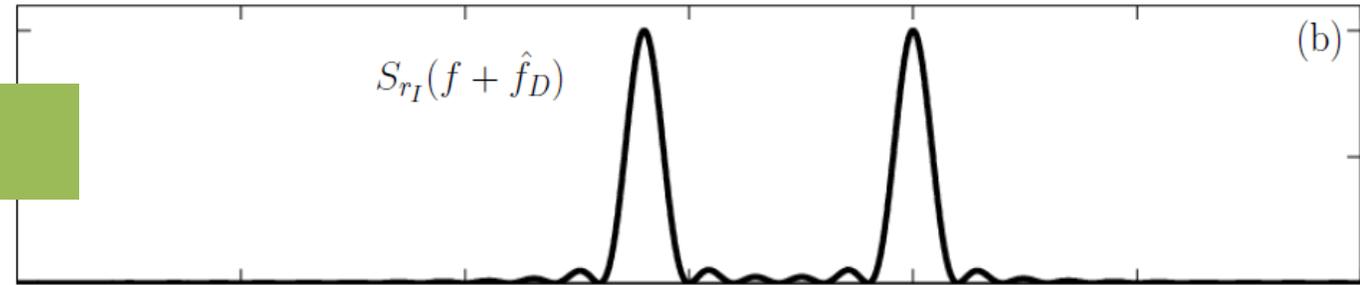
$$S_I(f) = S_{C_l}(f) \star S_{r_I}(f) \star \delta(f + \hat{f}_D)$$

Received signal is multiplied by a local replica and accumulated. In the frequency domain, the interference component of $Y(t)$ is a convolution of the psds of the desired code, the interference signal, and a delta fcn at the Doppler estimate.

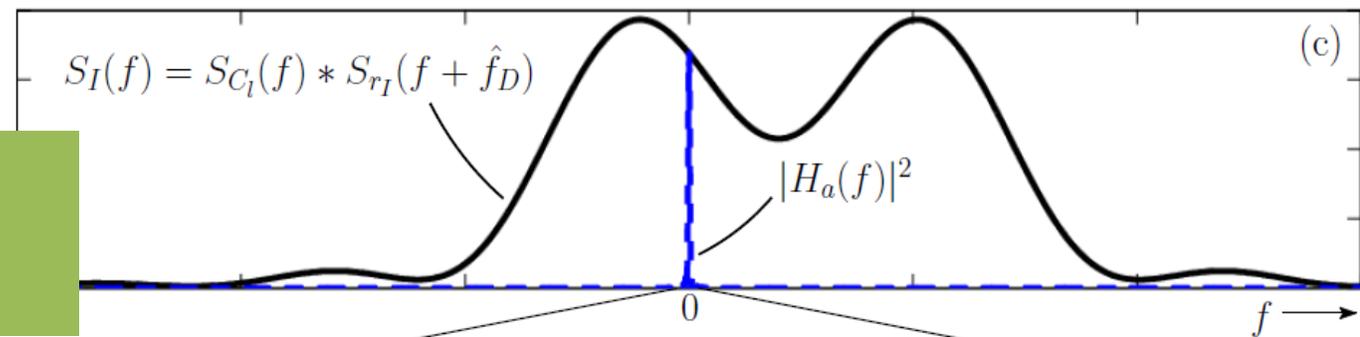
psd of desired signal's spreading code



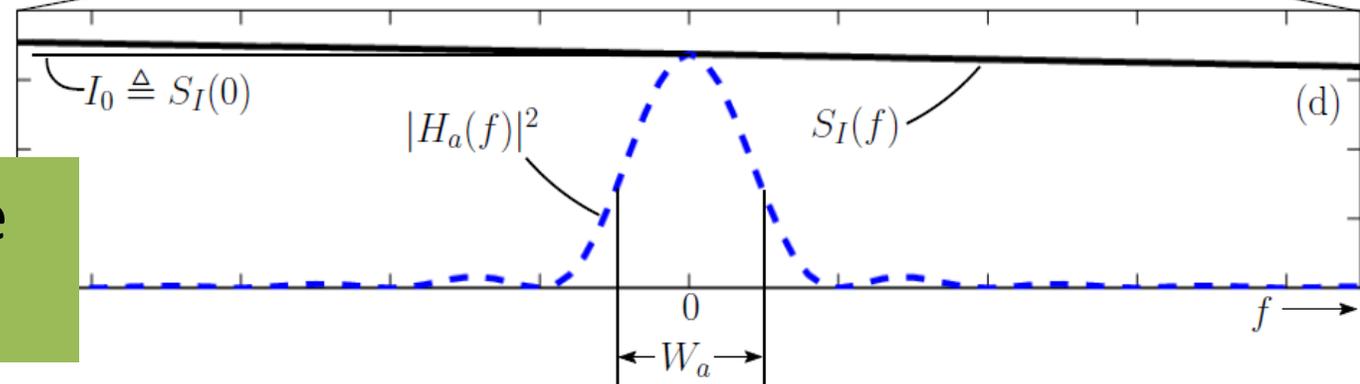
psd of interference signal



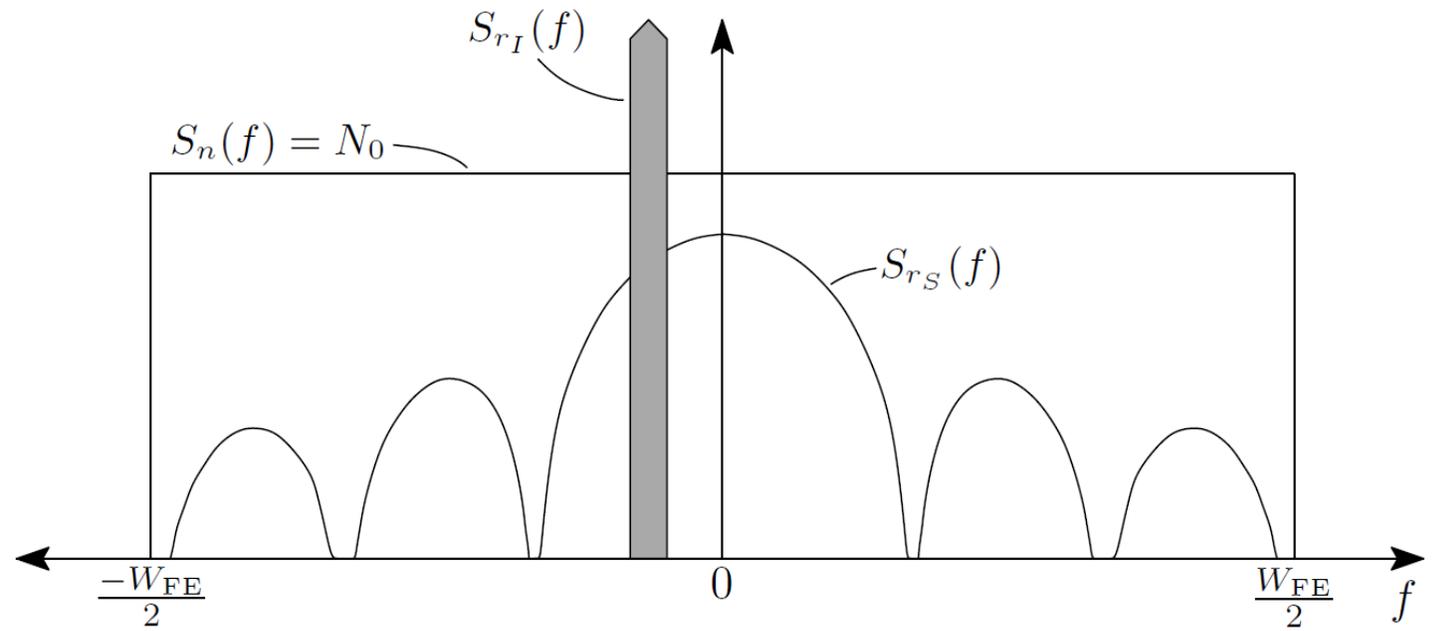
psd of $I(t)$, the interference component of $Y(t)$



I_0 is what makes it through into the receiver's tracking loops



$$\text{CINR}_i = \frac{P_i}{N_0 + M_{0i} + I_0}$$



$$I_0 := \int_{-W_{\text{FE}}/2}^{W_{\text{FE}}/2} S_{r_I}(f) S_{C_l}(f) df$$

$$M_{0i} = \frac{2T_C}{3} \sum_{j \in \mathcal{I}(t) \setminus i} P_{A_j}$$

Q: What waveform is most potent for jamming? In other words, for a fixed interference power P_I what S_{r_I} maximizes I_0 ?

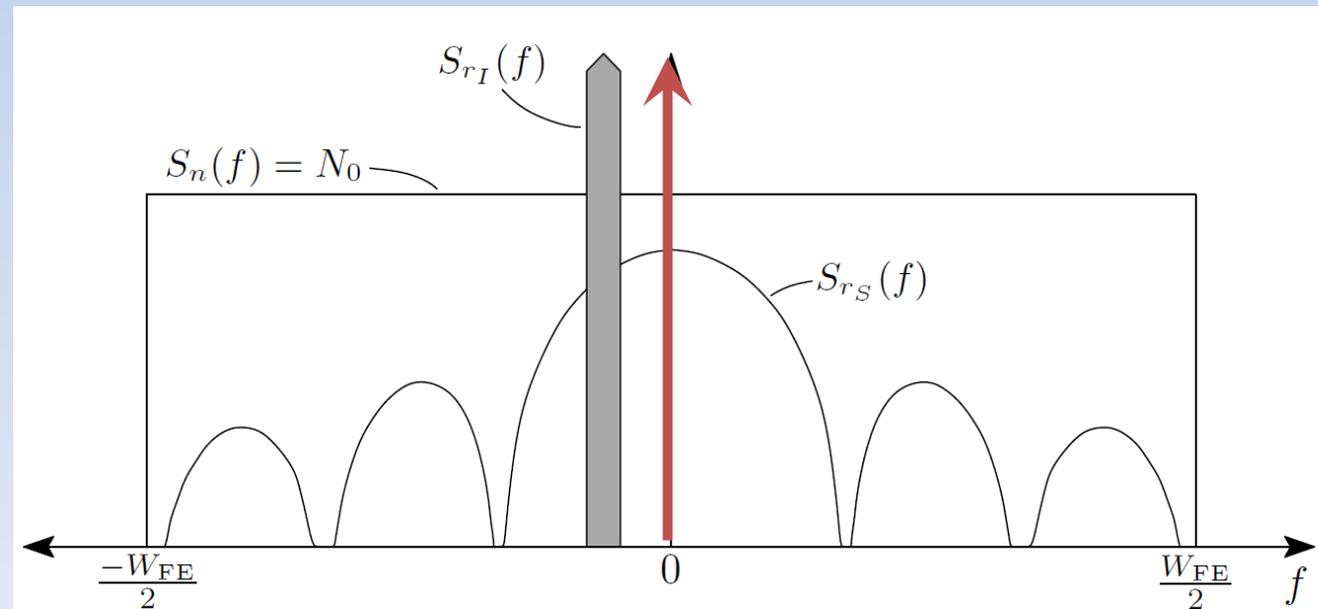
$$I_0 := \int_{-W_{FE}/2}^{W_{FE}/2} S_{r_I}(f) S_{C_l}(f) df$$

A: A pure tone jammer aligned with the highest point on the desired signal's psd:

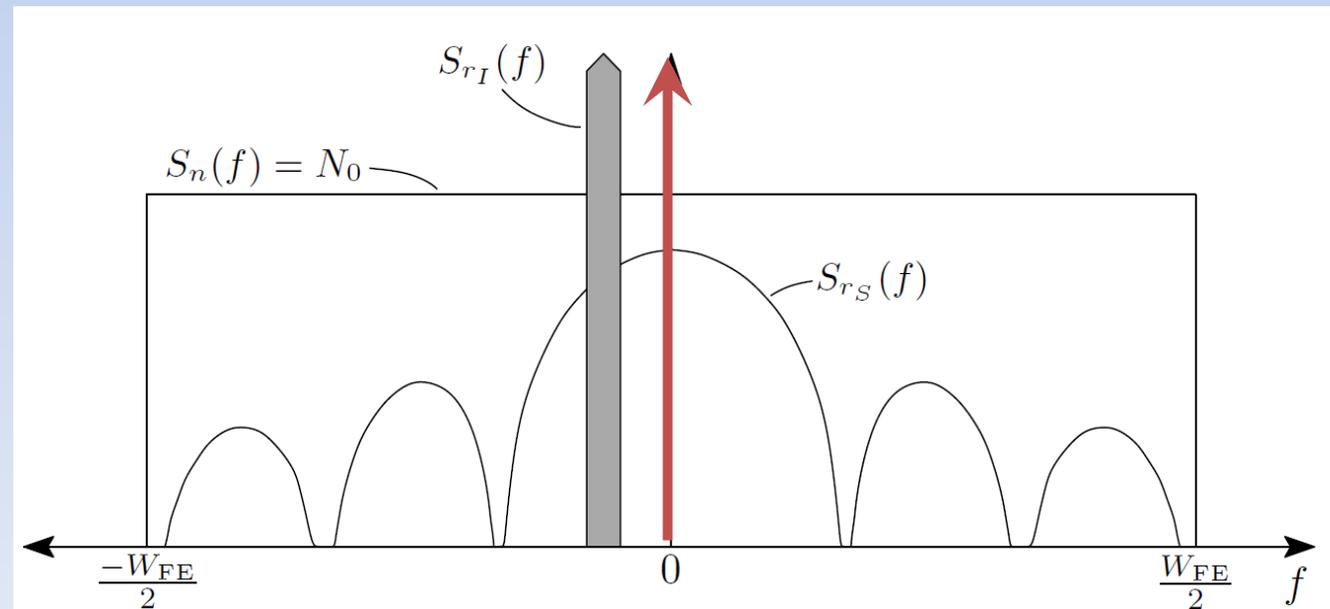
$$S_{r_I} = P_I \delta(\hat{f}_D)$$

$$I_0 := \int_{-W_{FE}/2}^{W_{FE}/2} S_{r_I}(f) S_{C_i}(f) df$$

$$\text{CINR}_i = \frac{P_i}{N_0 + M_{0i} + I_0}$$

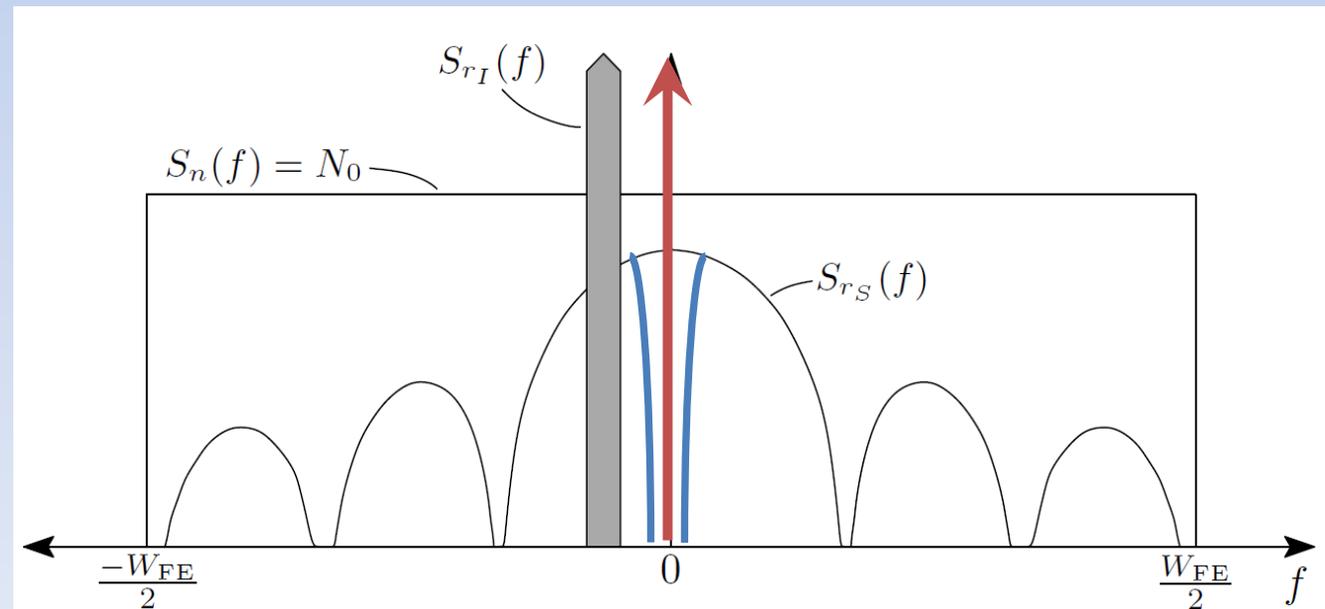


Q: Then why isn't the jammer in Syria using this most potent waveform?

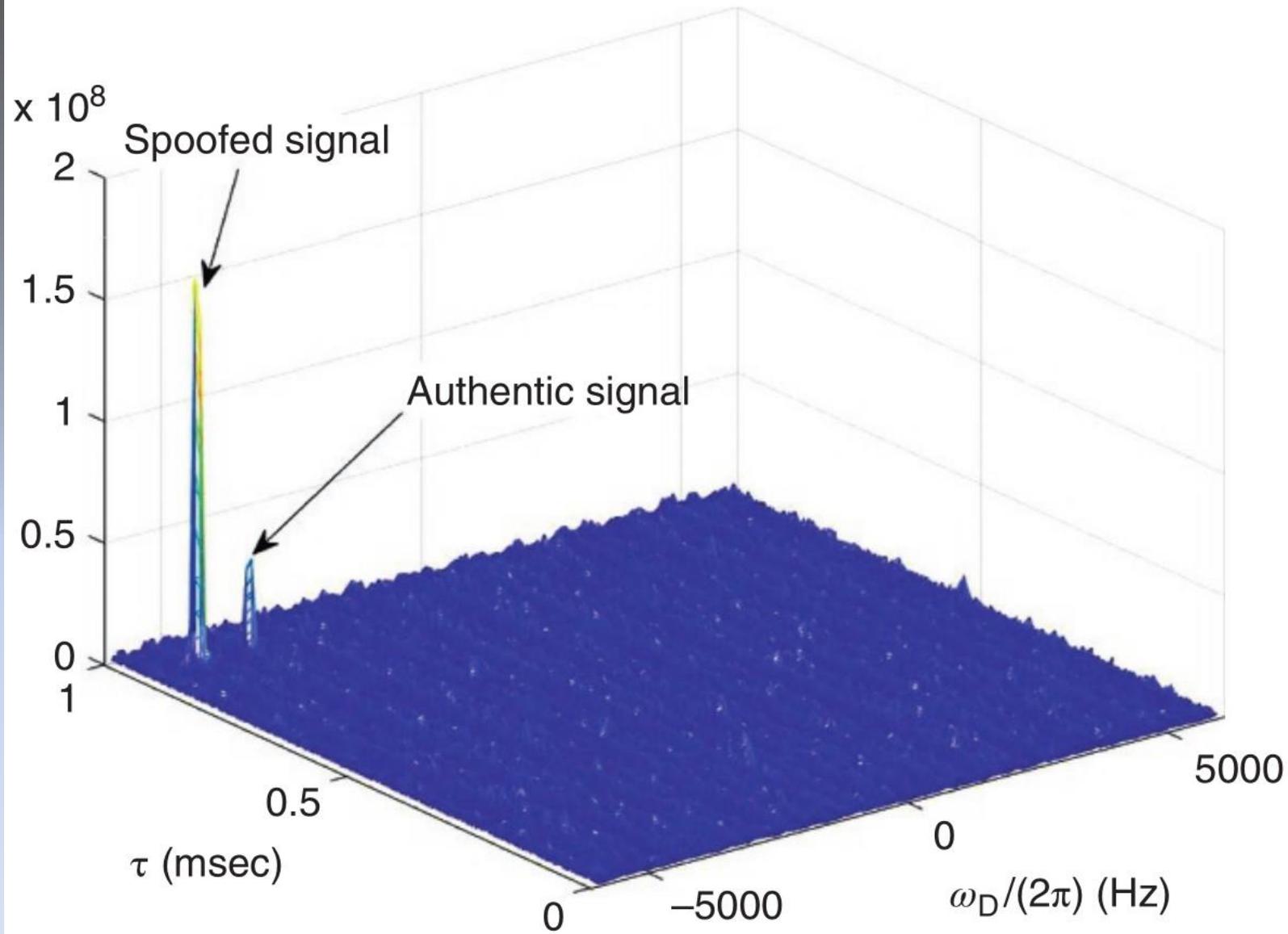


Q: Then why isn't the jammer in Syria using this most potent waveform?

A: It's too easy to defeat: a simple notch filter will do the trick.



To be both power-efficient and effective (hard to reject), the jamming signal has to produce high I_0 *but avoid being sparse in some domain* (e.g., time, frequency, code space, direction of arrival). A continuous matched-spectrum signal coming from multiple directions is both power-efficient and non-sparse (difficult to excise).



It takes very little interference power to present a cold-starting receiver with a conundrum: which peak does it choose?

Against civil receivers performing cold start, spoofing is more efficient for denial of service than jamming: a 1W spoofer is more potent than a 1kW matched-spectrum jammer at the same stand-off distance

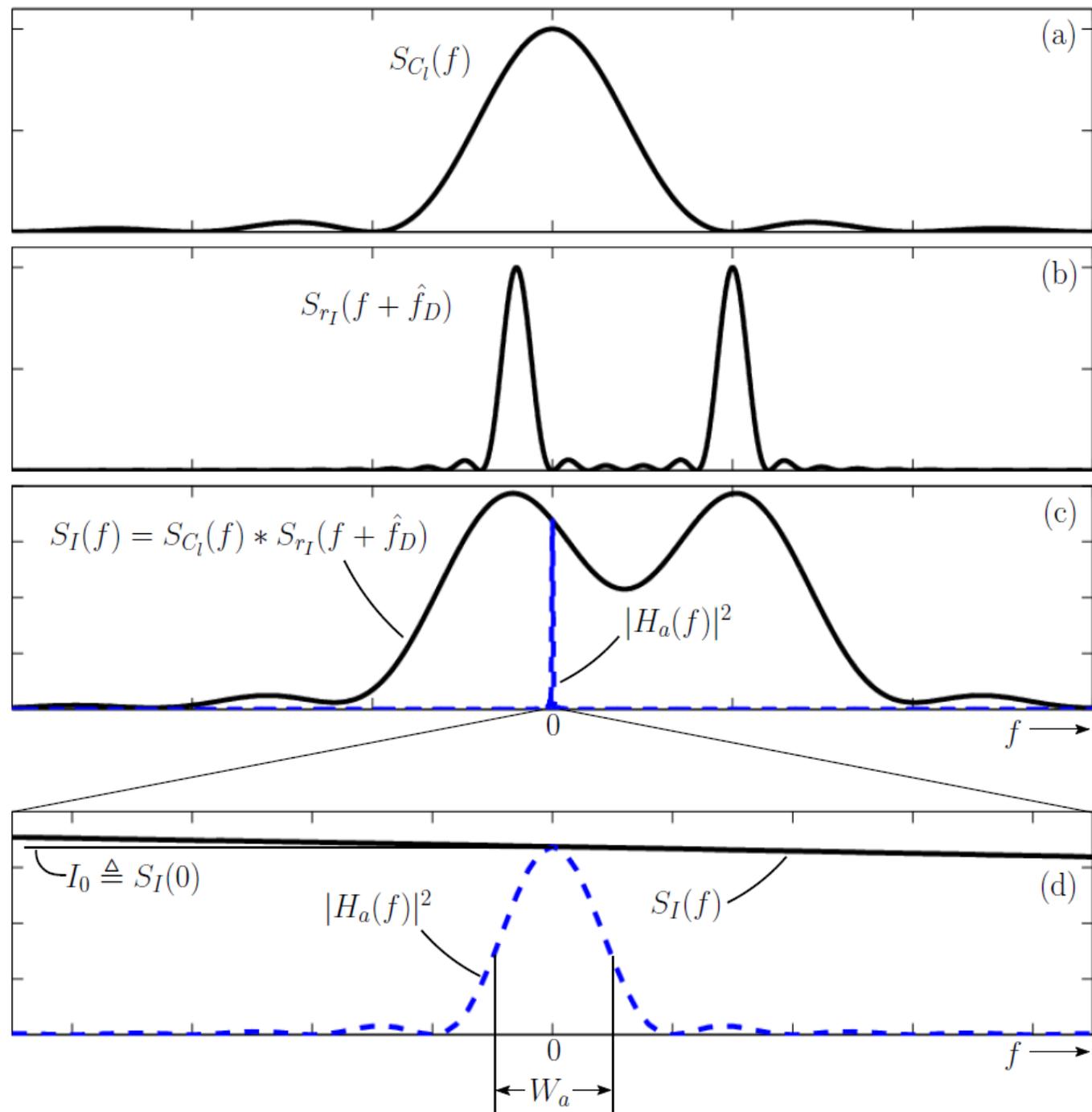
$$\frac{P_I}{C} = - \left[\eta + 10 \log_{10} \left(\frac{2T_C}{3} \right) \right]$$

For a typical CINR acquisition threshold of $\eta = 30$ dB-Hz, the received jamming-to-signal power ratio must be 31.8 dB to deny service. For DOS via spoofing it need only be 0 dB.

Q: What desired-signal spreading code is most effective for resisting interference? In other words, what S_{C_l} minimizes I_0 ?

$$I_0 := \int_{-W_{FE}/2}^{W_{FE}/2} S_{r_I}(f) S_{C_l}(f) df$$

A: The wider the better. M-Code BOC(10,5) is an excellent example.



Q: How do we build a resilient PNT box?

Q: First, how do we authenticate GNSS signals?

There are many spoofing detection and mitigation techniques. None is perfect. The practical objective is to price your adversary out of the game.

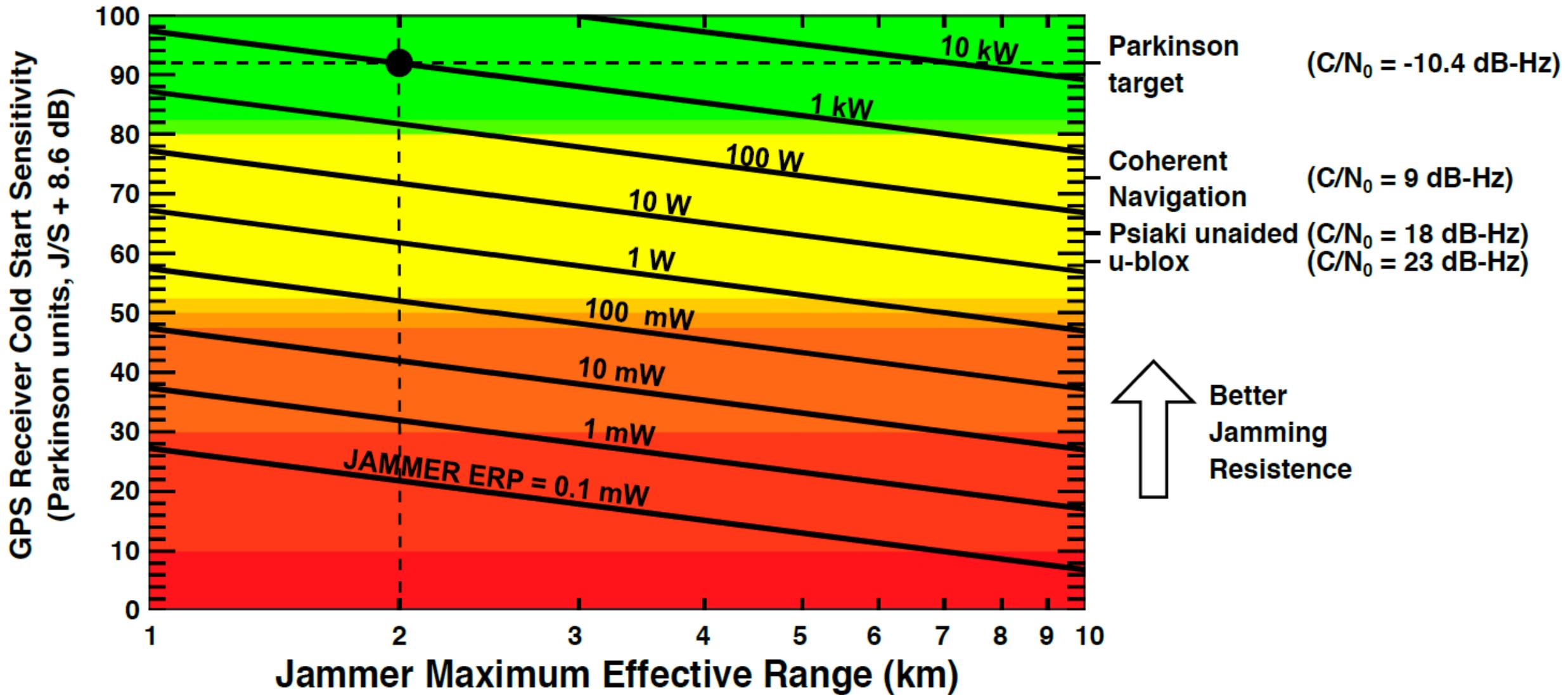
Psiaki, Mark L., and Todd E. Humphreys. "GNSS spoofing and detection." *Proceedings of the IEEE* 104.6 (2016): 1258-1270.

TABLE I: Cost-Ranked Matrix of GNSS Spoofing Attack and Detection Techniques

Detection Techniques	Attack Techniques												
	A1	A2	A3	A4	A5	A6	A7	A8	A9	A10	A11	A12	A13
D1	X	X	X	X	X	X	X	X	X	X	X	X	X
D2	~	✓	X	X	~	X	X	X	X	X	~	X	X
D3	~	~	~	~	~	X	X	~	~	~	~	X	X
D4	~	✓	~	~	~	~	~	~	~	~	~	~	~
D5	✓	✓	✓	✓	✓	~	~	✓	✓	✓	✓	~	~
D6	X	✓	✓	X	X	✓	X	✓	✓	X	X	✓	X
D7	X	✓	✓	~	X	✓	~	✓	✓	~	X	✓	~
D8	X	✓	✓	✓	X	✓	✓	✓	✓	✓	X	✓	✓
D9	~	✓	✓	✓	~	✓	✓	✓	✓	✓	~	✓	✓
D10	✓	✓	✓	✓	✓	✓	✓	✓	~	~	~	~	~
D11	✓	✓	✓	✓	✓	✓	✓	X	~	~	~	~	~
D12	X	✓	✓	✓	X	✓	✓	✓	✓	✓	X	✓	✓
D13	X	✓	✓	✓	X	✓	✓	✓	✓	✓	X	✓	✓

Attack Techniques Key		Detection Techniques Key	
A1	Meaconing, single RX ant., single TX ant.	D1	Pseudorange-based RAIM
A2	Open-loop signal simulator	D2	Observables and RPM
A3	RX/SP, single TX ant., no SCER	D3	Correlation fcn. distortion monitoring
A4	RX/SP, single TX ant., SCER	D4	Drift monitoring (clock offset, IMU/position)
A5	Meaconing, multi. RX ants., single TX ant.	D5	Observables, RPM, distortion, and drift monitoring
A6	Nulling RX/SP, single TX ant., no SCER	D6	NMA*
A7	Nulling RX/SP, single TX ant., SCER	D7	NMA* and SCER detection
A8	RX/SP, single TX ant., sensing of victim ant. motion	D8	Asymmetric-key SSSC*
A9	RX/SP, mult. TX ants., no SCER	D9	NMA*, SCER detection, RPM, and drift monitoring
A10	RX/SP, mult. TX ants., SCER	D10	Multiple RX antennas
A11	Meaconing, multi. RX ants., multi. TX ants.	D11	Moving RX antenna
A12	Nulling RX/SP, mult. TX ants., no SCER	D12	Dual-RX correlation of P(Y) or M codes
A13	Nulling RX/SP, mult. TX ants., SCER	D13	Symmetric-key SSSC* [e.g., P(Y) equiv.]

Q: Next, how do we prevent denial of PNT?



PTA: By (1) deep coupling with inertial sensors, and (2) multi-element antennas we can toughen GNSS receivers enough to withstand 1 kW wideband Gaussian jammer at a distance of 2 km.



Robust, precise, high-integrity PNT for self-driving cars



University of Texas Sensorium

Emphasis on high-integrity PNT: Precise dual-antenna GNSS, three radar units, stereo cameras, inertial sensing, stable internal clock, LTE comms.

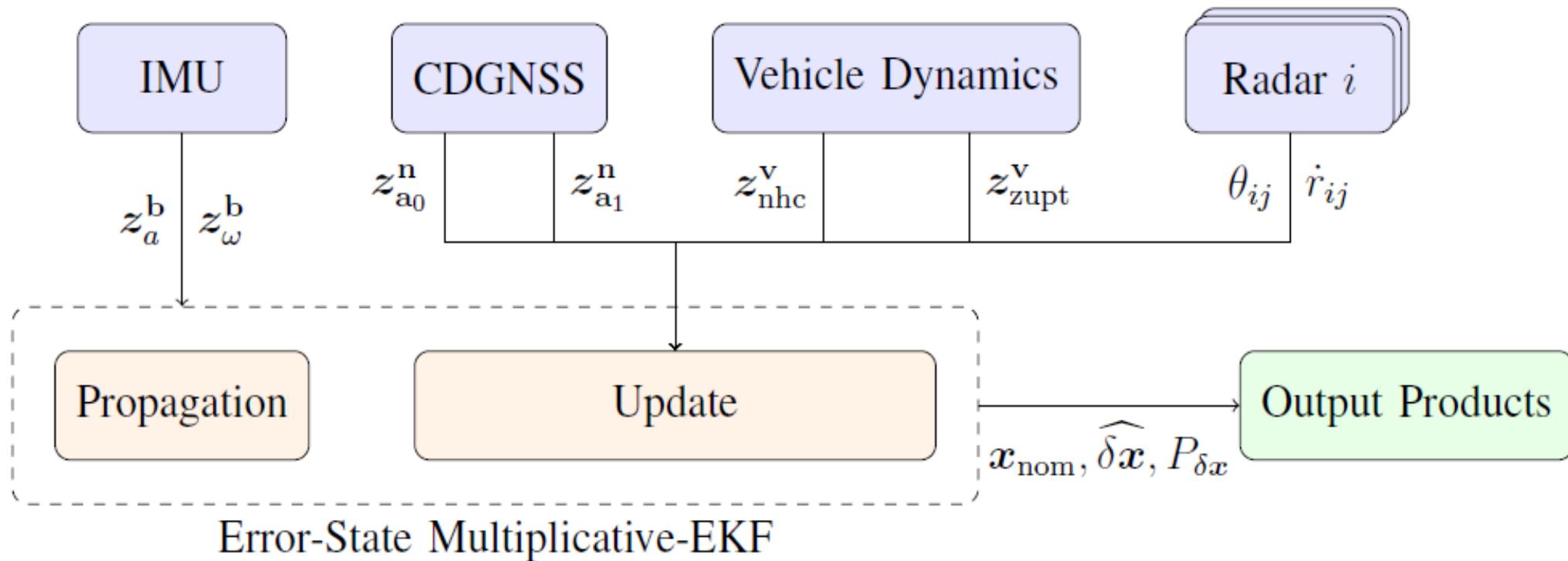
Ground Truth:

Forward-backward smoothed solution from iXblue ATLANS-C connected to the test antenna

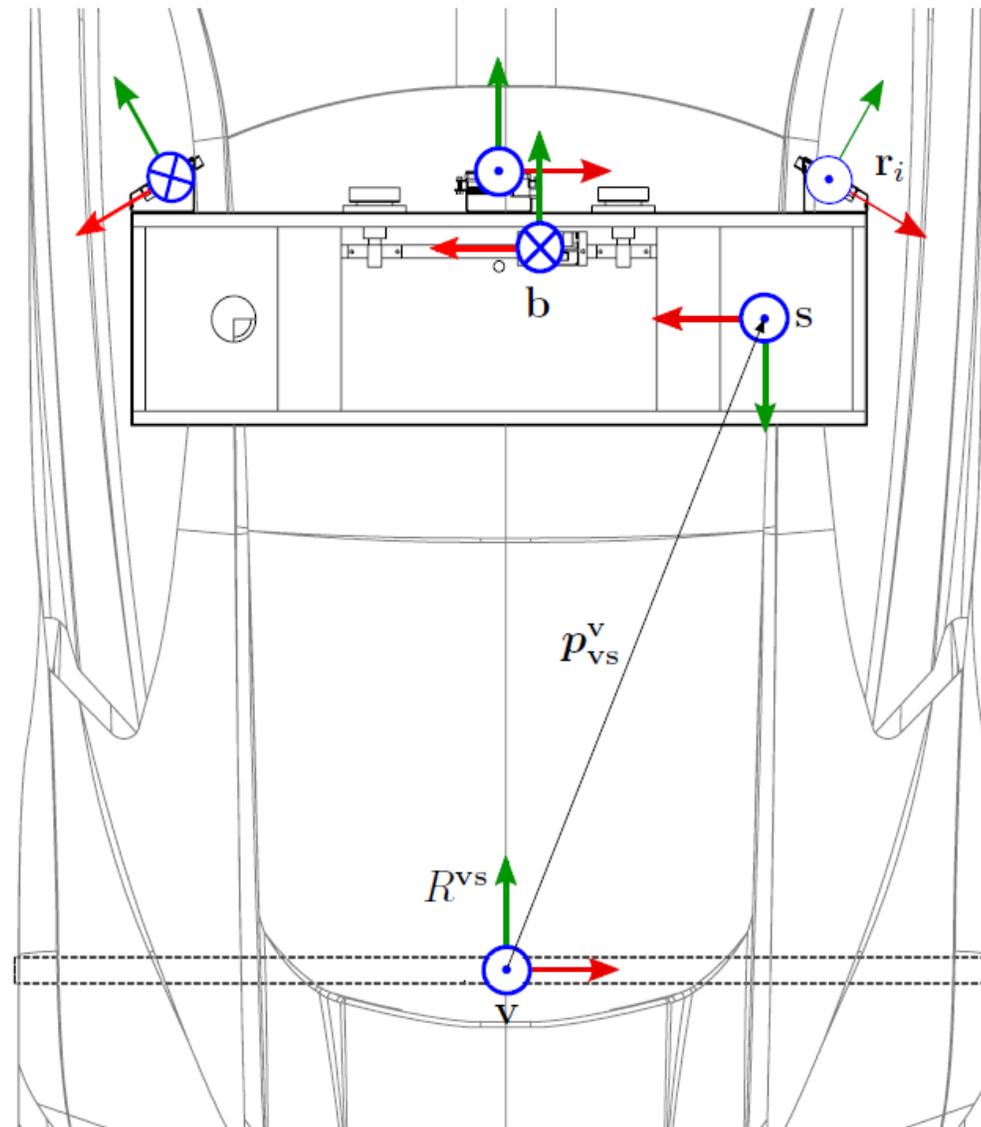
The ATLANS-C “smartly” couples a tactical-grade IMU with a Septentrio RTK receiver

1-sigma reported uncertainty ranged from 2cm to 20cm

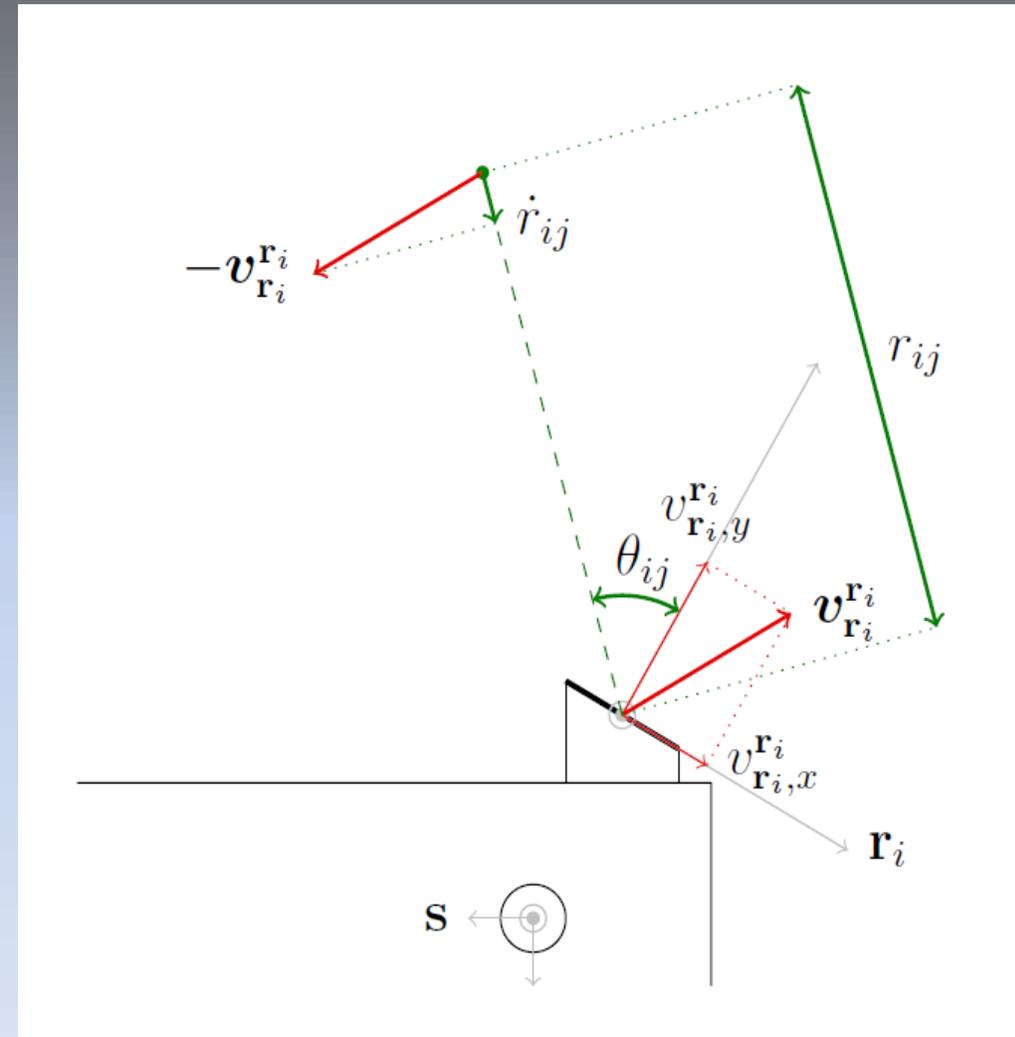
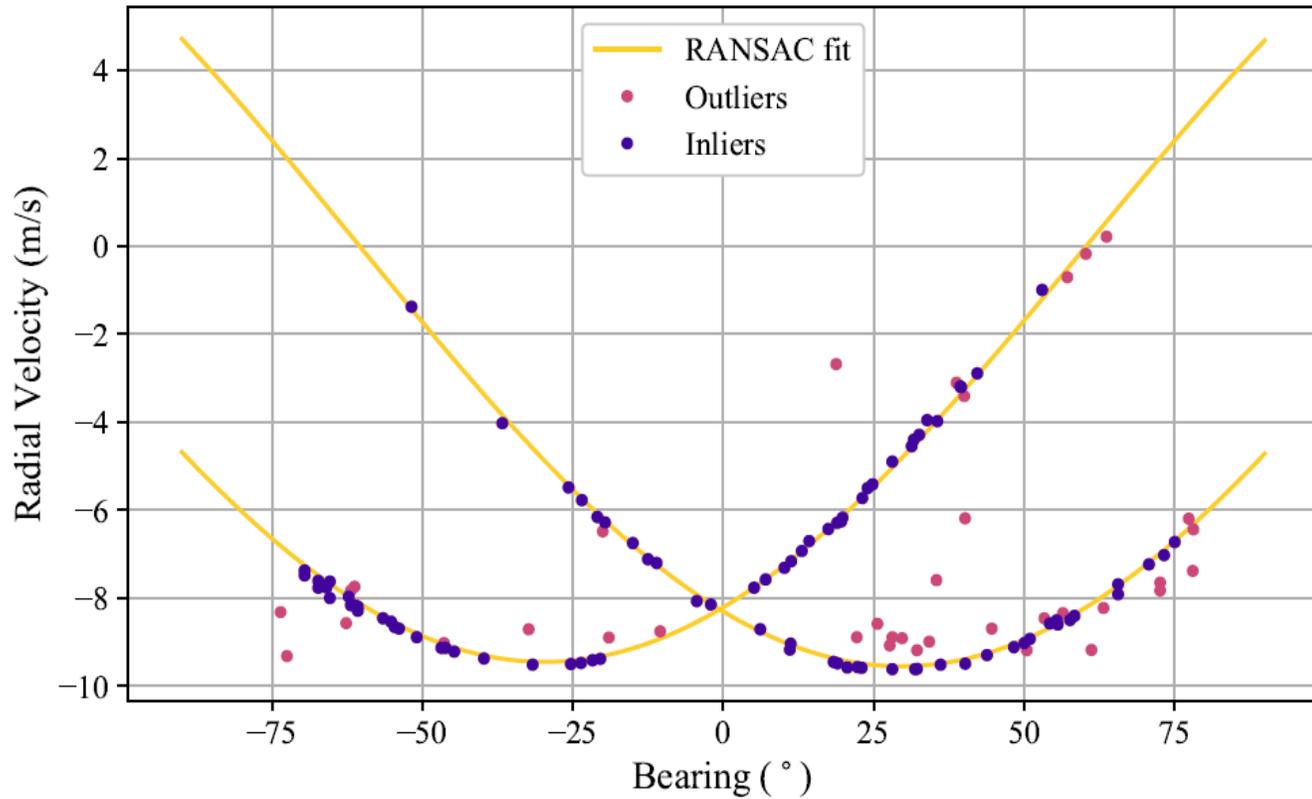




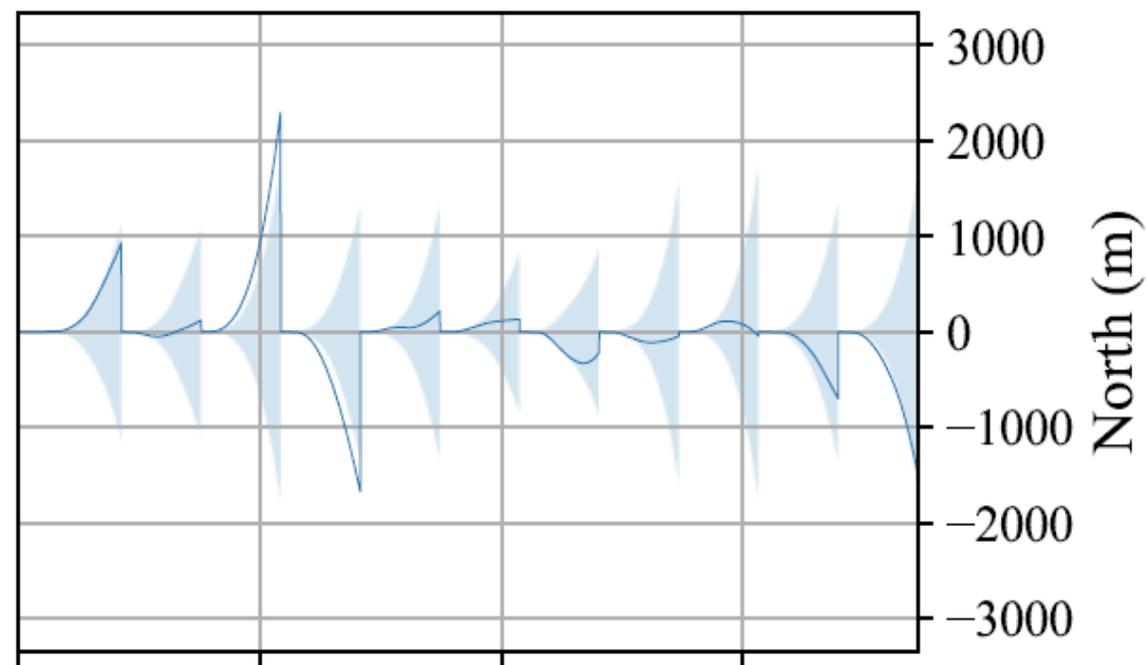
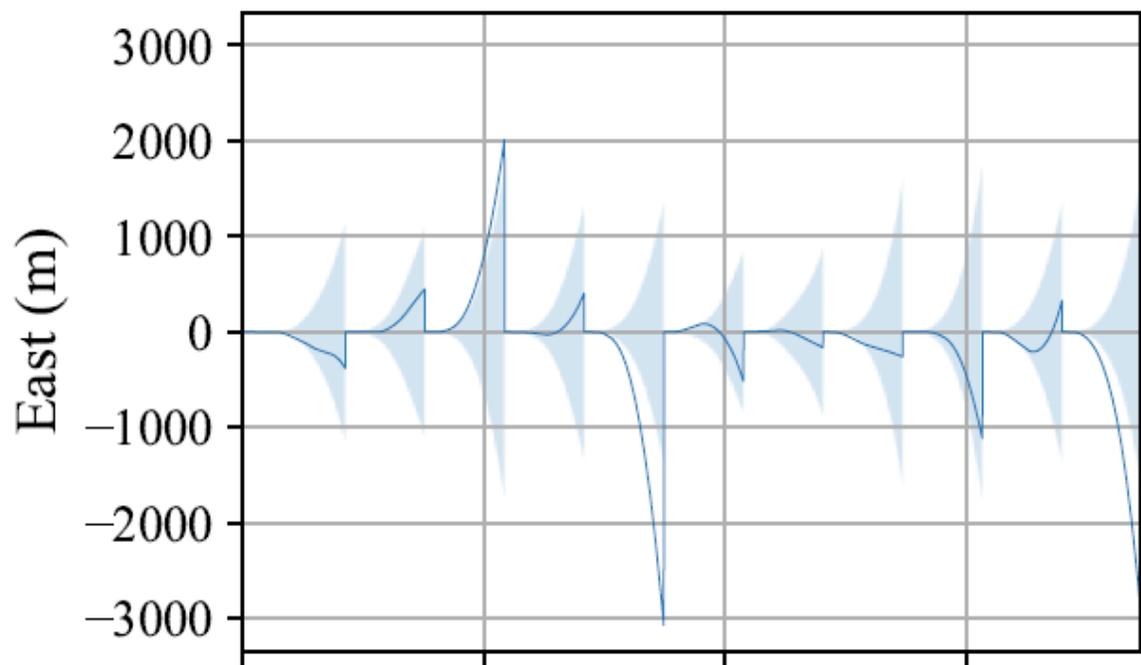
CDGNSS (when available), vehicle dynamics, and radar are fused to constrain drift of IMU



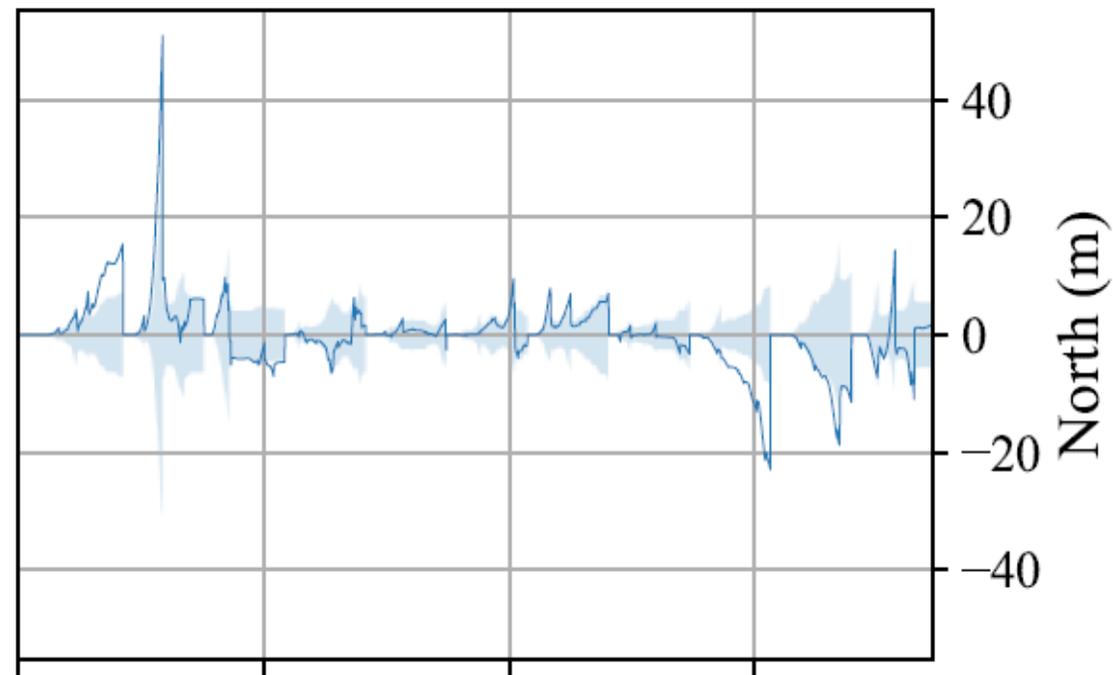
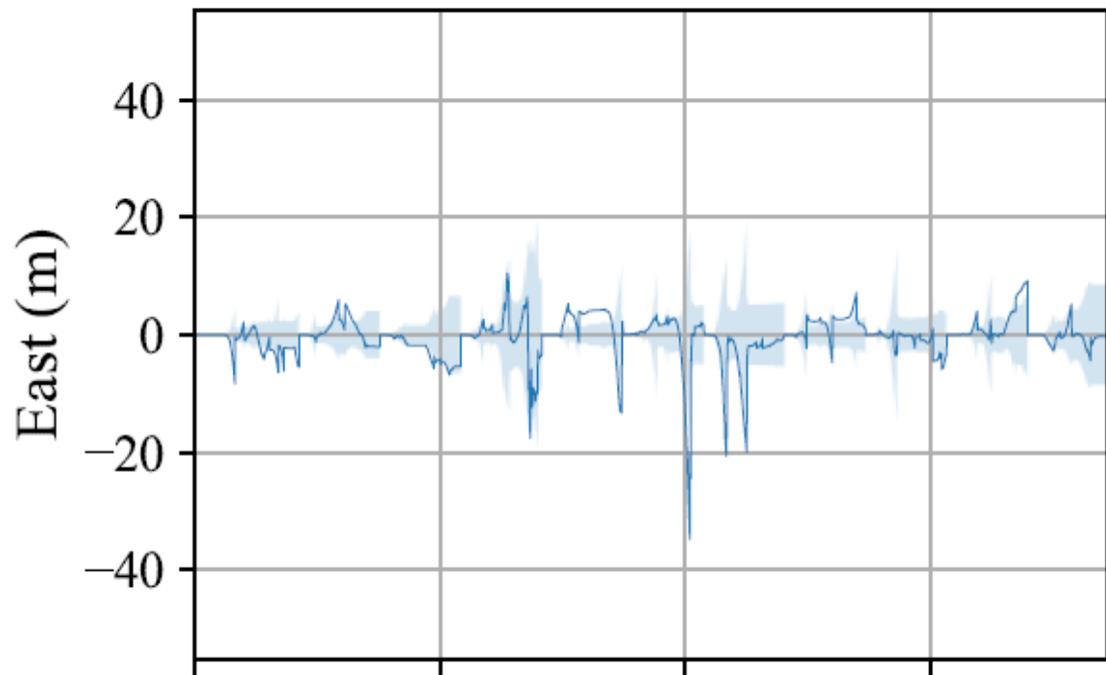
Must determine vehicle's center of rotation
in order to apply zero-sideslip constraint



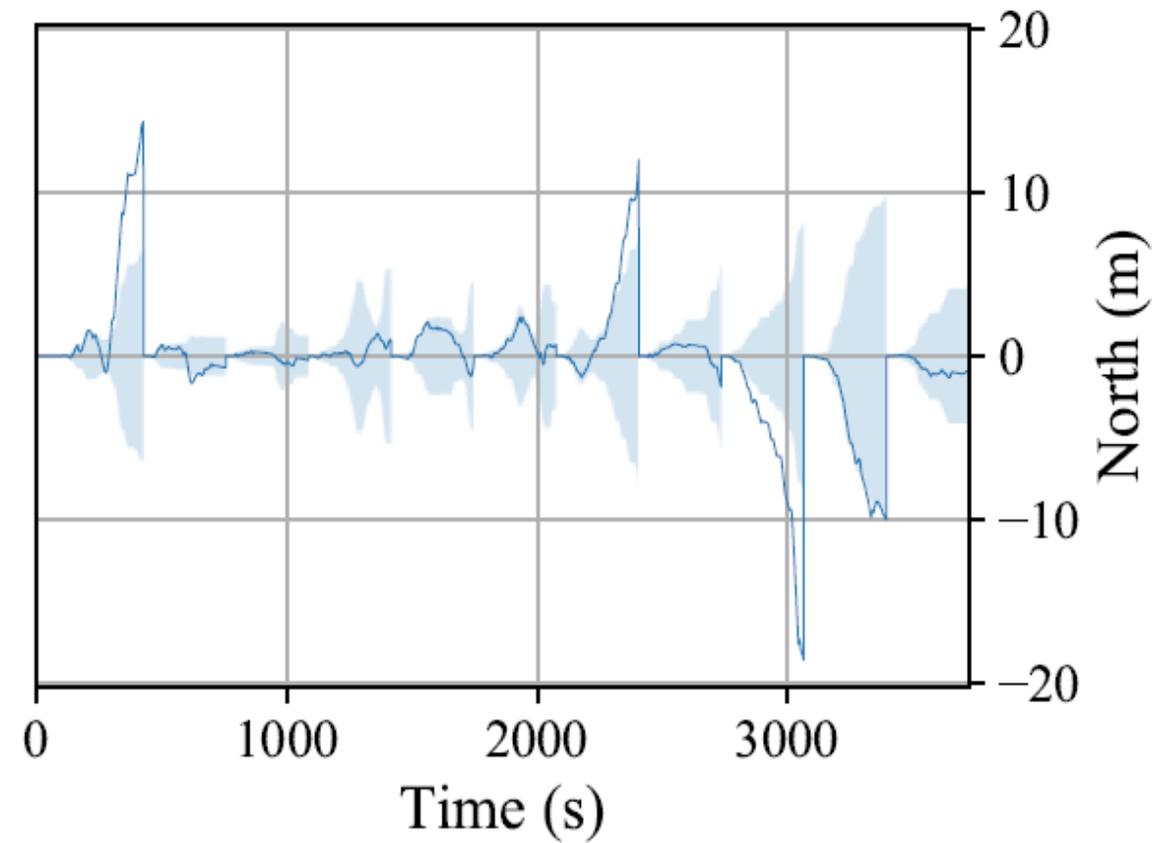
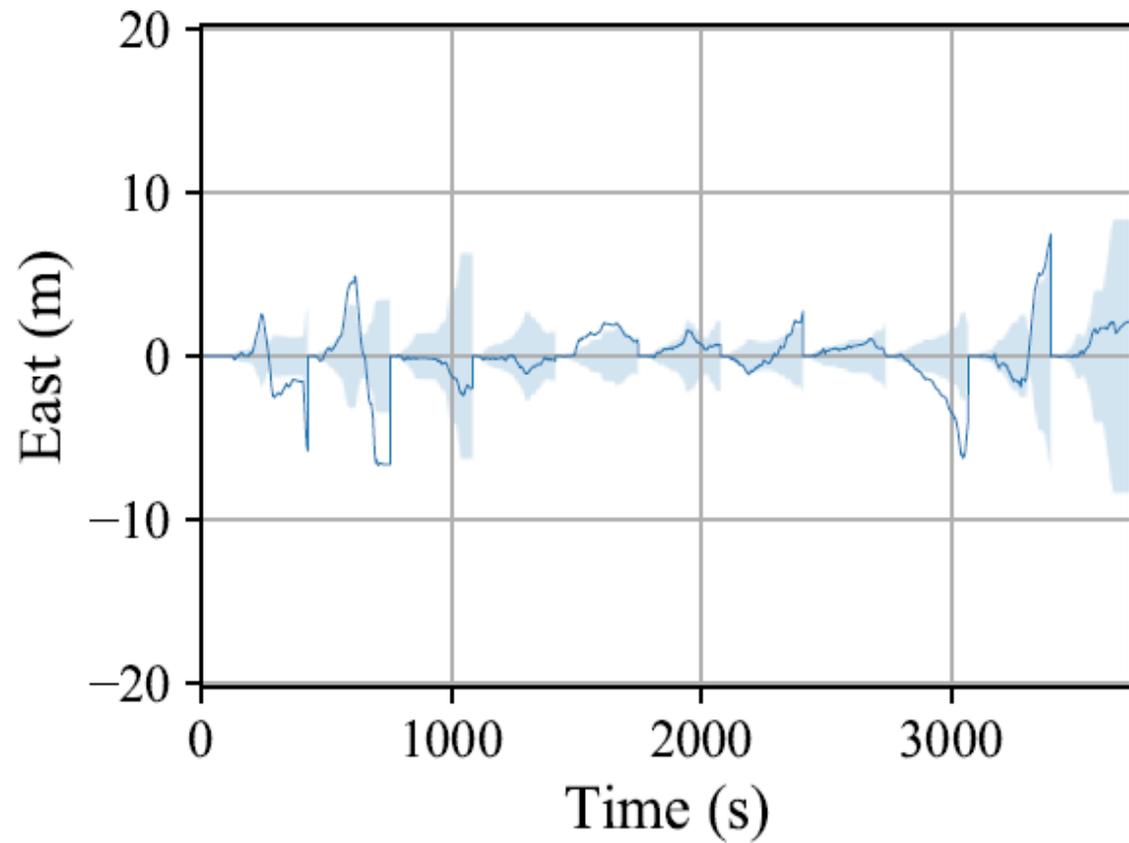
Must model and calibrate radar sensors



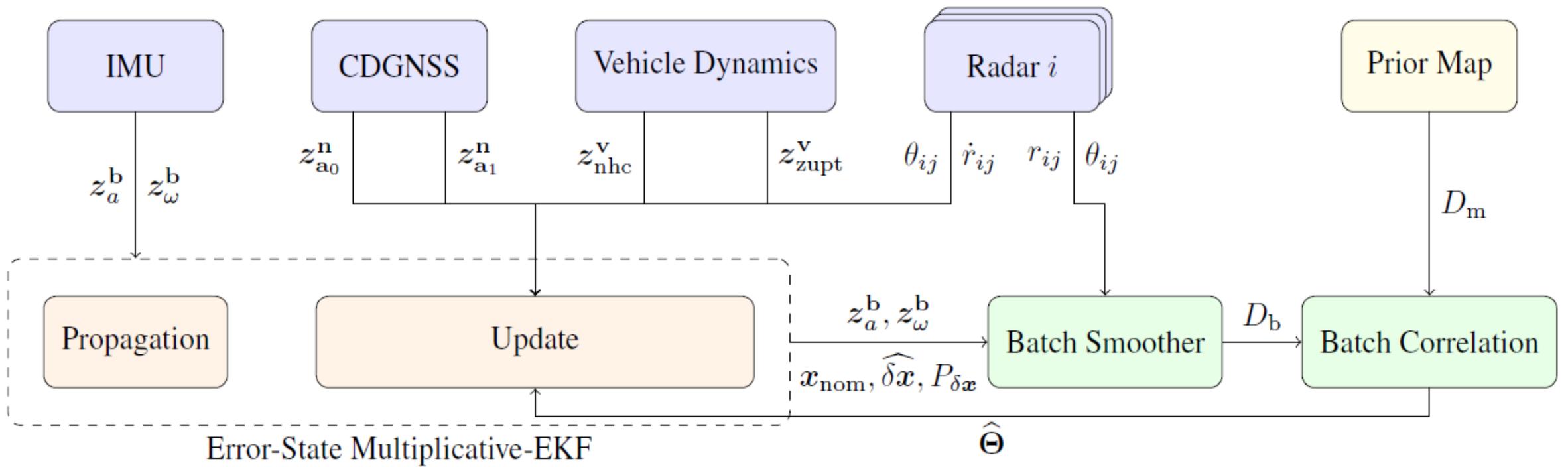
Periodic 5-minute GNSS outages:
High-end MEMS IMU drifts up to 2km



Now with vehicle motion model constraints (zero sideslip, ZUPD).
High-end MEMS IMU drifts less than 40 meters.

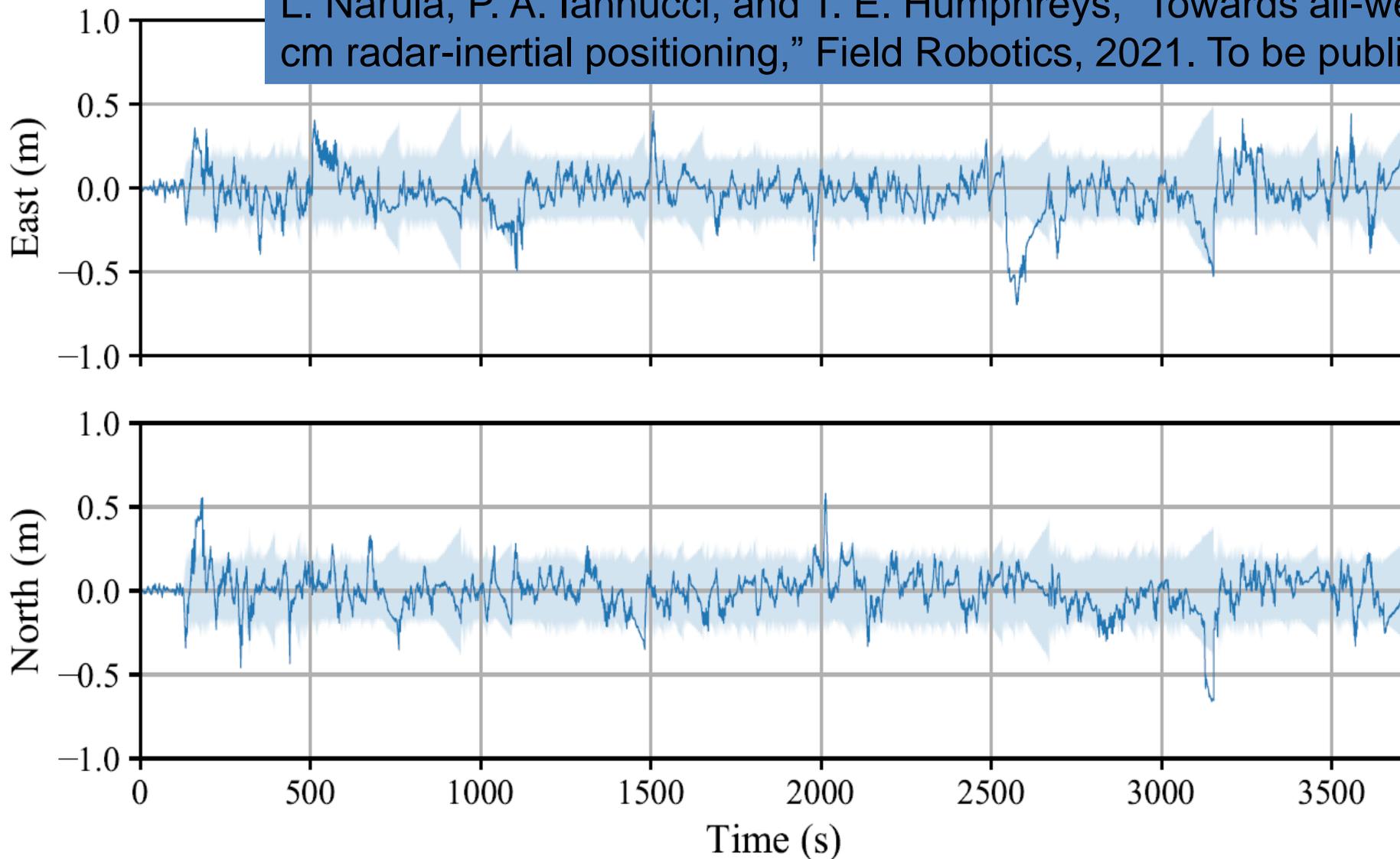


Additionally with radar range rate constraints (no prior map).
High-end MEMS IMU drifts less than 20 meters.



Further constrain with a prior radar map

L. Narula, P. A. Iannucci, and T. E. Humphreys, "Towards all-weather sub-50-cm radar-inertial positioning," Field Robotics, 2021. To be published.



A prior radar map enables 60-minute GNSS-denied vehicle positioning to better than 0.5 meters.

T. E. Humphreys, *Interference*, pp. 469-503. Springer International Publishing, 2017

Psiaki, Mark L., and Todd E. Humphreys. "GNSS spoofing and detection." *Proceedings of the IEEE* 104.6 (2016): 1258-1270.

M. L. Psiaki and T. E. Humphreys, *Position, Navigation, and Timing Technologies in the 21st Century: Integrated Satellite Navigation, Sensor Systems, and Civil Applications*, vol. 1, ch. Civilian GNSS Spoofing, Detection, and Recovery, pp. 655-680. Wiley-IEEE, 2020

L. Scott, *Position, Navigation, and Timing Technologies in the 21st Century: Integrated Satellite Navigation, Sensor Systems, and Civil Applications*, vol. 1, ch. Interference: Origins, Effects, Mitigations, pp. 619-654. Wiley-IEEE, 2020

L. Narula, P. A. Iannucci, and T. E. Humphreys, "Towards all-weather sub-50-cm radar-inertial positioning," *Field Robotics*, 2021. To be published.

M. J. Murrian, L. Narula, P. A. Iannucci, S. Budzien, B. W. O'Hanlon, S. P. Powell, and T. E. Humphreys, "First results from three years of GNSS interference monitoring from low Earth orbit," *Navigation, Journal of the Institute of Navigation*, 2021. Submitted for review.

T. E. Humphreys, M. J. Murrian, and L. Narula, "Deep-urban unaided precise global navigation satellite system vehicle positioning," *IEEE Intelligent Transportation Systems Magazine*, vol. 12, no. 3, pp. 109-122, 2020



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